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# Initial Thinking on the ReBCO Based R&D Program at BNL for USMDP

MDP Videoconference on June 5, 2019

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for Magnet Division at BNL

# **Purpose of the BNL Program (as stated in the FWP for USMDP)**

- ❖ **Develop very high field magnet technologies based on Nb<sub>3</sub>Sn and HTS.**
- ❖ **Take advantage of the unique test bed based on the existing 10 T Nb<sub>3</sub>Sn common dipole DCC017 with a large open space.**
  - ✓ **Facilitate a rapid-turn-around, low cost high field test facility for carrying out innovative and/or systematic R&D with new racetrack insert coils becoming an integral part of the magnet without requiring disassembly of the background field magnet.**
  - ✓ **Utilize the unique geometry of the dipole DCC017 providing background field of 10 T to perform quench, magnetization and other studies of partial to several turns of high current cables, including those requiring large bend radii.**

- 1. Magnetization studies (@4K, up to 10 T) in an HTS coil with field primarily parallel to the wide face of the ReBCO tape**
  - 2. Quench studies in a few turn coil made with CORC cable**
- **Funding became available in late May.**
  - **We hope to finish these tasks by the end of this year, definitely by April 2020 (within a year).**

# Initial Thinking

## Carryout both tasks in parallel

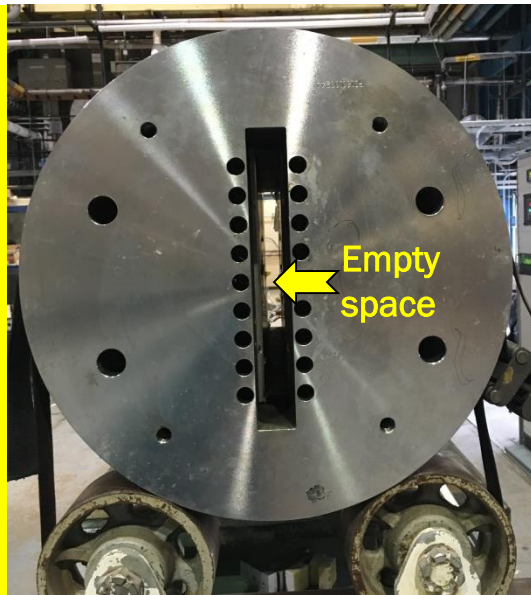
1. Start on task #1: Conductor (HTS tape) is available for winding new coils now. The test setup for this task requires minimum upgrade since the last experiment when the HTS tape coils were tested with field primarily perpendicular to the wide face. Initial studies started.
2. Design/discussion on task#2: CORC coil requires a significant design, planning and interaction with collaborators, in addition to the cable. Upgrade in test setup (independent higher current in CORC insert coil), though not essential, would enhance the test program. Status/progress and initial thoughts will be presented.



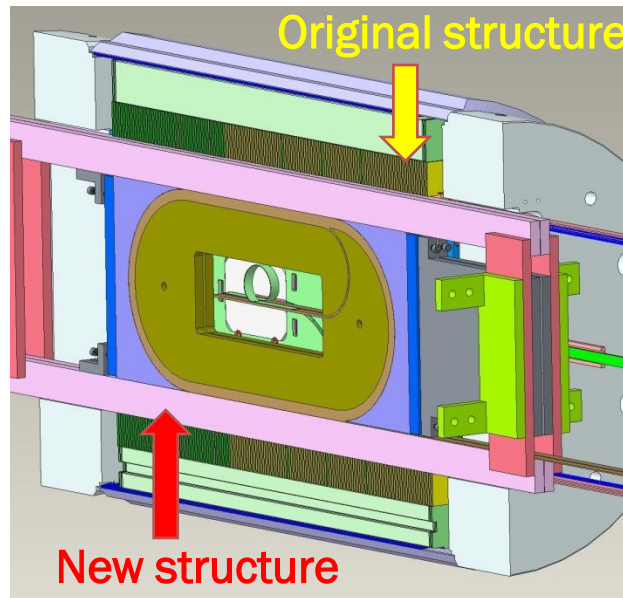
# The Test Bed: DCC017

## A unique feature of BNL's common coil dipole:

- large open space for inserting & testing “coils” without any disassembly (rapid around, lower cost)



BNL Nb<sub>3</sub>Sn common coil dipole DCC017 without insert coils



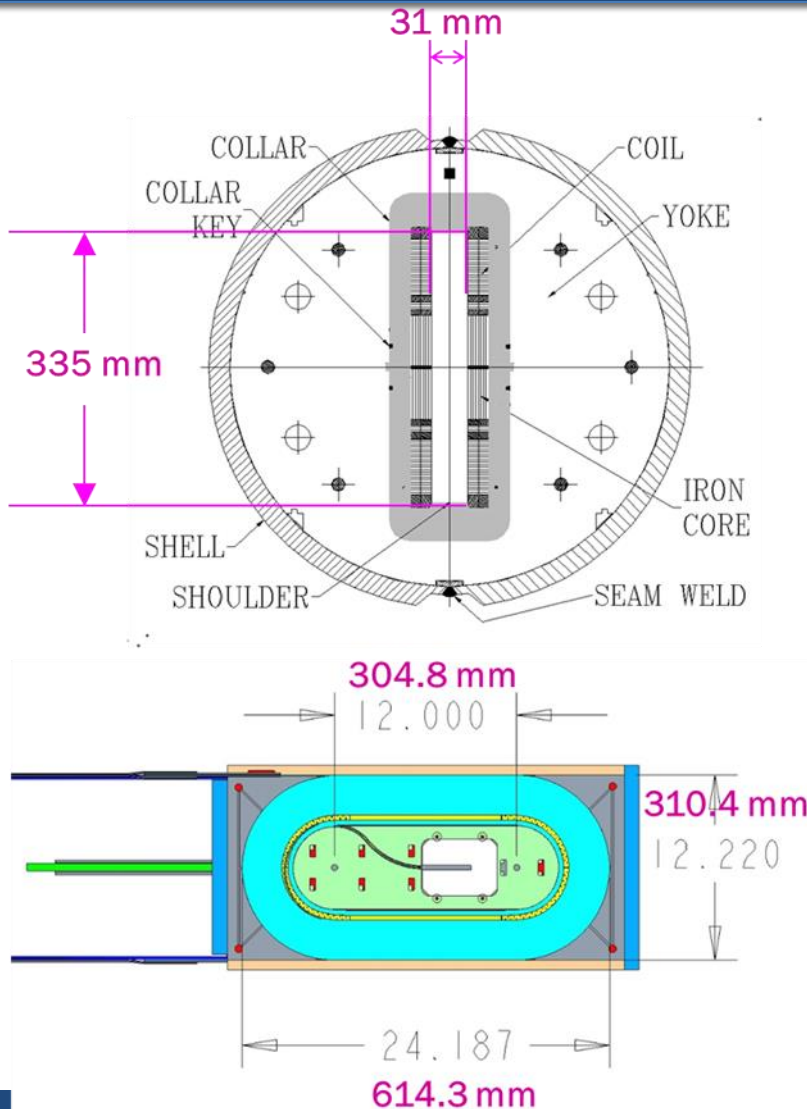
New HTS coils with the existing Nb<sub>3</sub>Sn coils and become part of the magnet



HTS coils inside Nb<sub>3</sub>Sn dipole - early experience of HTS/LTS hybrid dipole



# Parameters of BNL Dipole DCC017



- Two layer, 2-in-1 common coil design
- 10.2 T bore field, 10.7 T peak field at 10.8 kA short sample current
- **31 mm horizontal aperture**
- **335 mm vertical aperture**
  - **A unique feature for insert coil or cable testing**
- 0.8 mm, 30 strand Rutherford cable
- 70 mm minimum bend radius
- 85 mm coil height
- 614 mm coil length
- One spacer in body and one in ends
- Iron over ends
- Iron bobbin
- Stored Energy @ Quench ~0.2 MJ



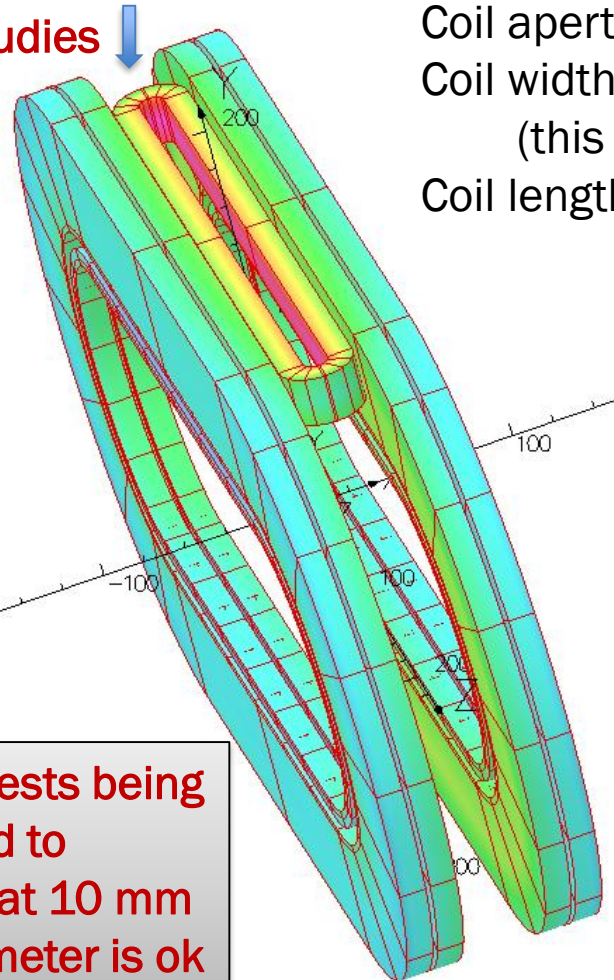
# Preparation/Planning for Task #1

1/Nov/2014 16:34:00

**HTS insert coil for field  
parallel studies**

Surface contours: BMOD

1.890129E+001  
1.800000E+001  
1.600000E+001  
1.400000E+001  
1.200000E+001  
1.000000E+001  
8.000000E+000  
6.000000E+000  
4.000000E+000  
1.817547E+000



**Bending tests being  
performed to  
ensure that 10 mm  
bend diameter is ok**

Gap for insert coil: 31 mm

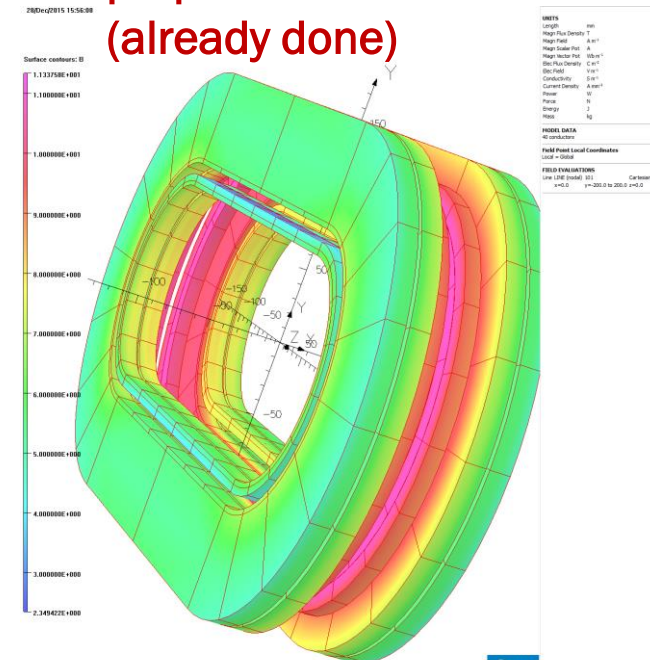
Coil aperture (minimum bend diameter): 10 mm

Coil width: 10 mm

(this allows 1 mm for insulation/clearances)

Coil length: ~300 mm

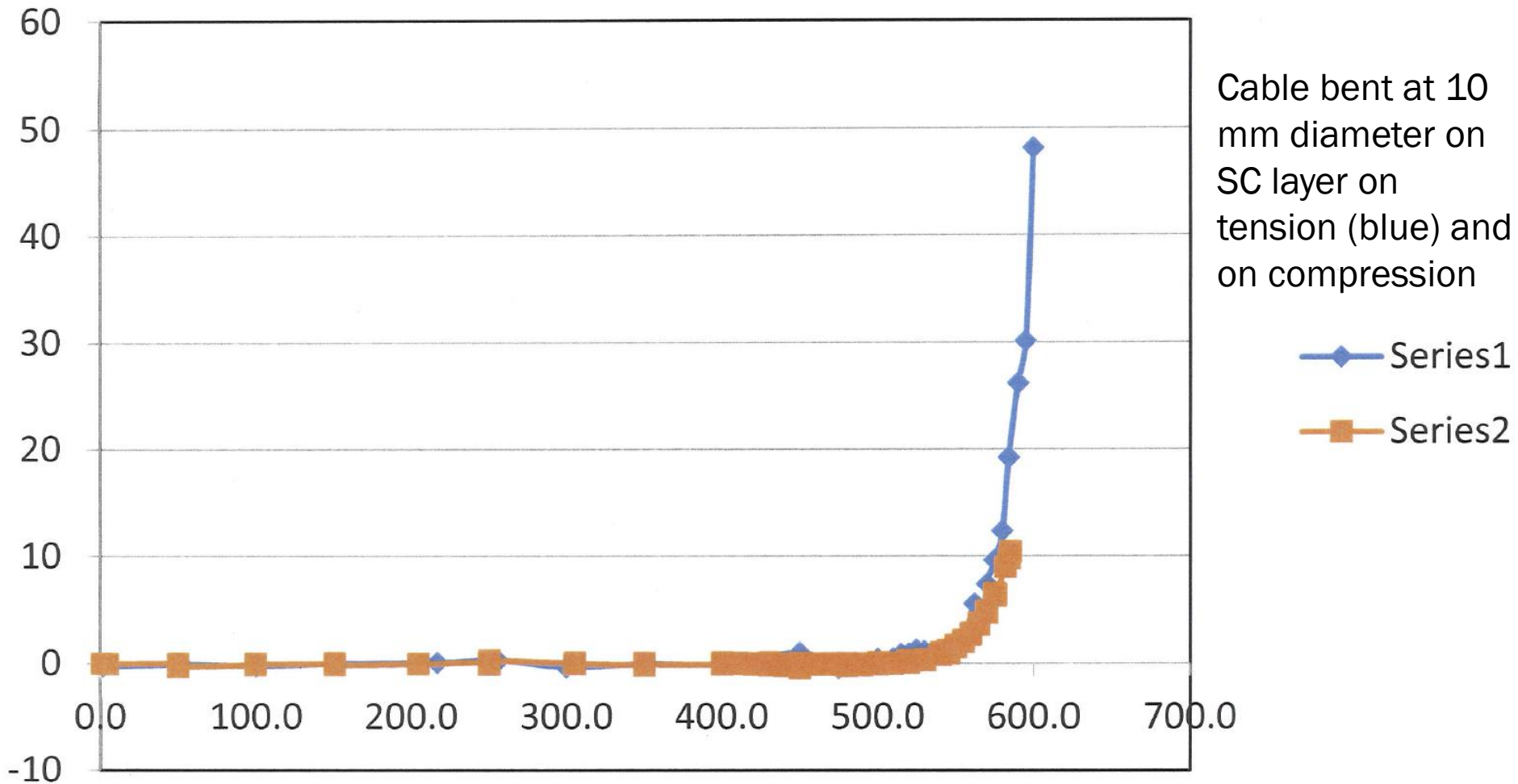
**HTS insert coil for field  
perpendicular studies  
(already done)**



Opera



# Plot from Bill Sampson (inserted <30 minutes ago)





## Basic Configuration:

- Two apertures allow two types of coils
- One coil with full Nomex insulation
- Another coil with “No” or “Partial” insulation (no insulation in the end region - ~ 5cm or so non-insulated region)

## Goals:

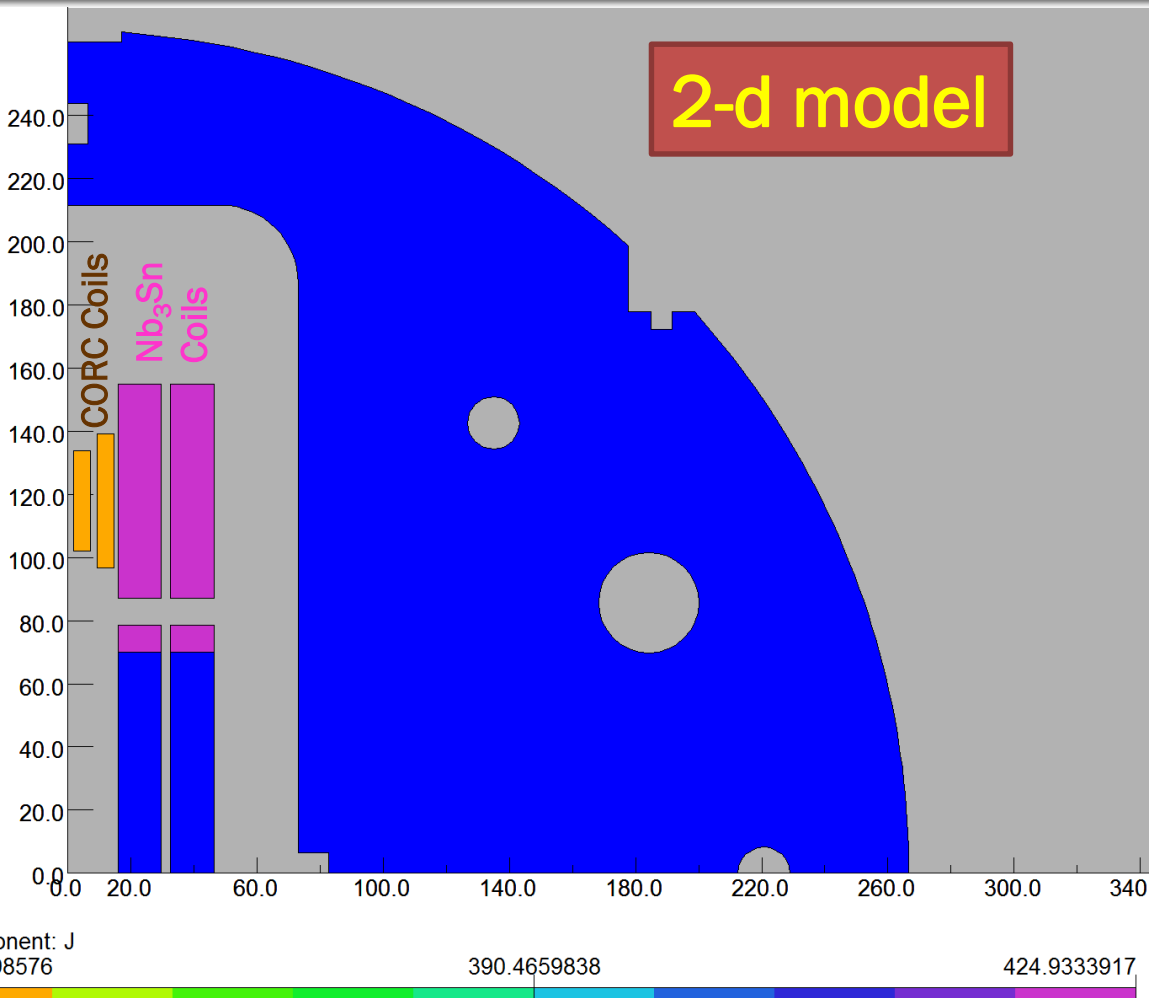
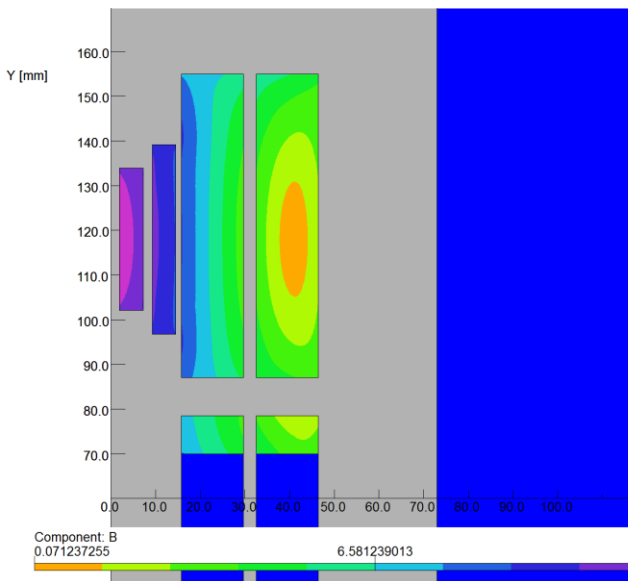
- Basic: Measure magnetization at various applied fields
- Additional: Perform quench studies (requires more planning)
  - What do we want to study?
  - Instrumentations?
  - Allow coil to be destroyed?
  - Impact of partial insulation on field quality and quench protection

# CORC Coils in the STTR Program

## CORC coils:

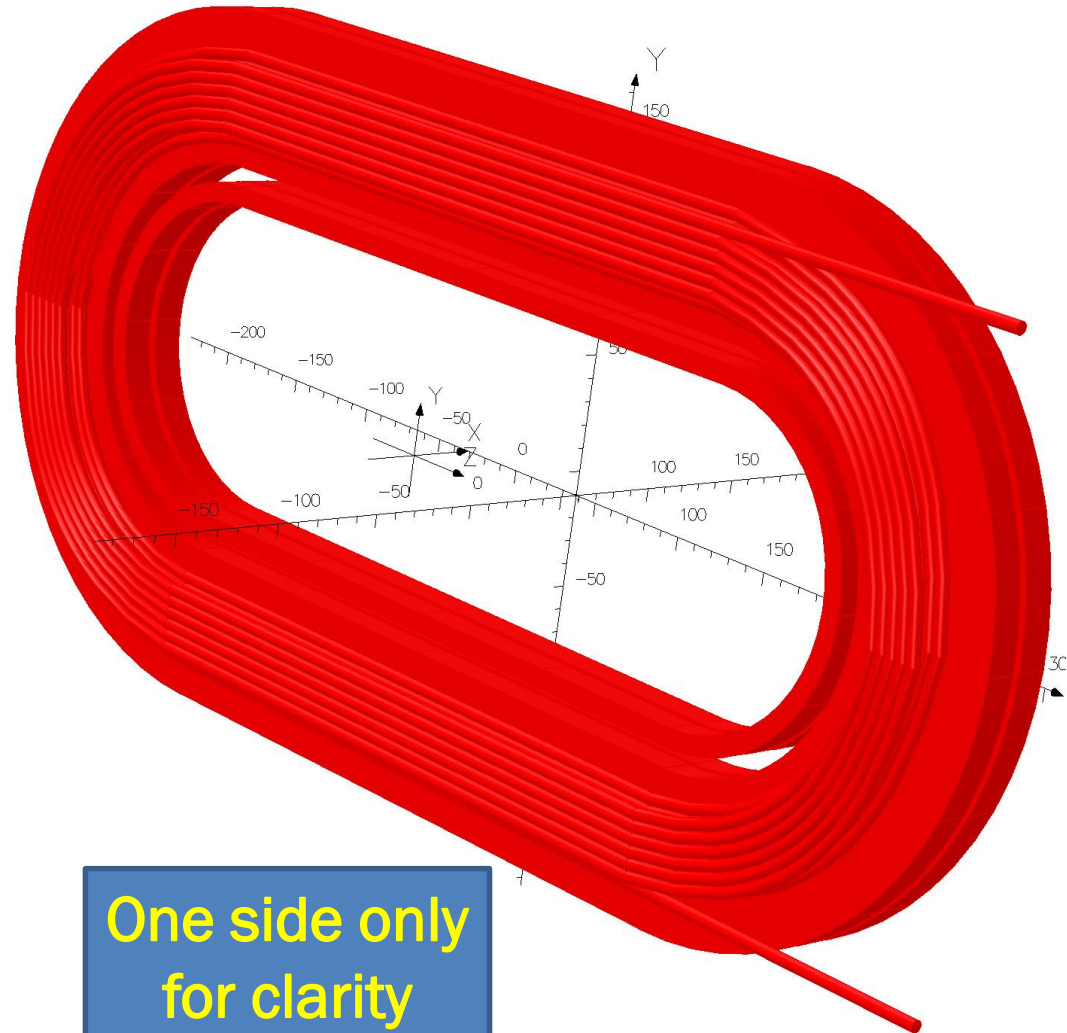
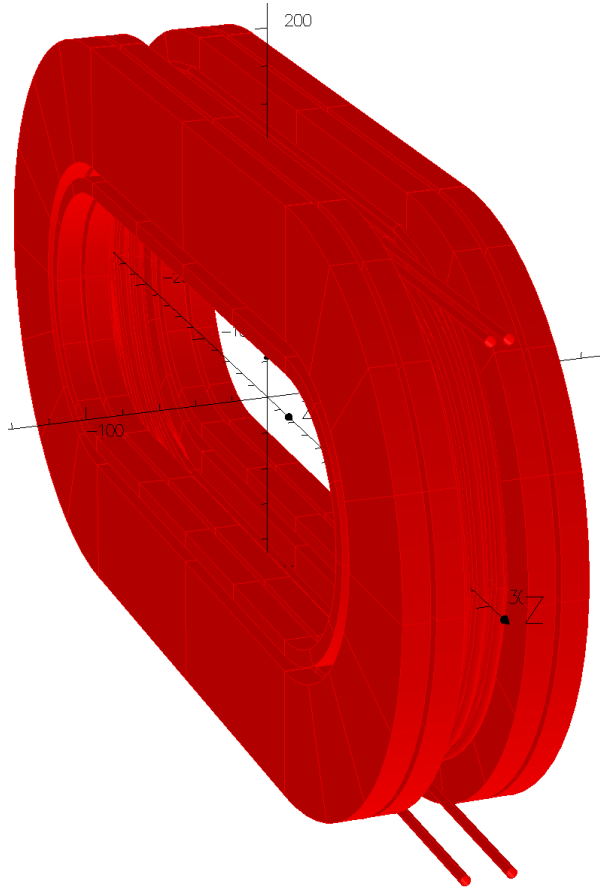
6 and 8 turns, running  
in series with Nb<sub>3</sub>Sn coils

Hybrid field: 13.1 T @10 kA  
: 14.4 T @11 kA  
(peak field in Nb<sub>3</sub>Sn coils  
reduced by CORC coils)





# CORC Coils (with 6 and 8 turns) inside the Nb<sub>3</sub>Sn coils

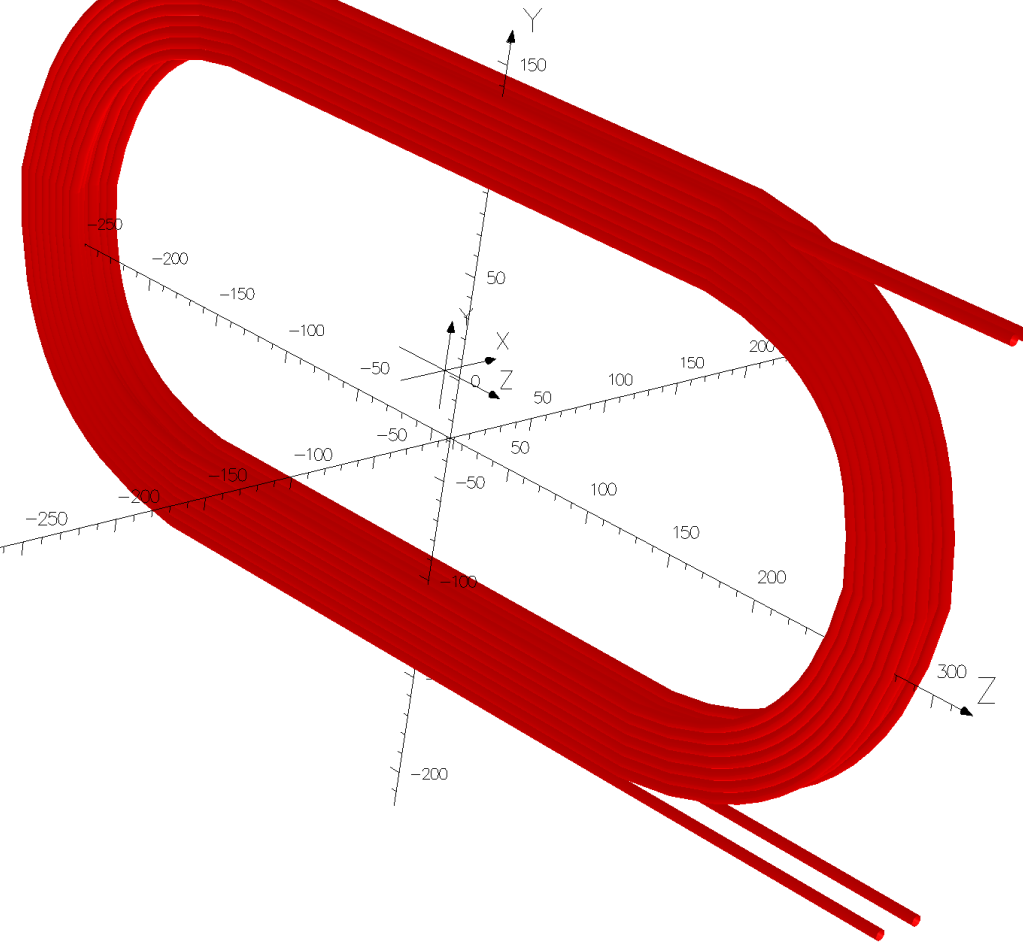


One side only  
for clarity

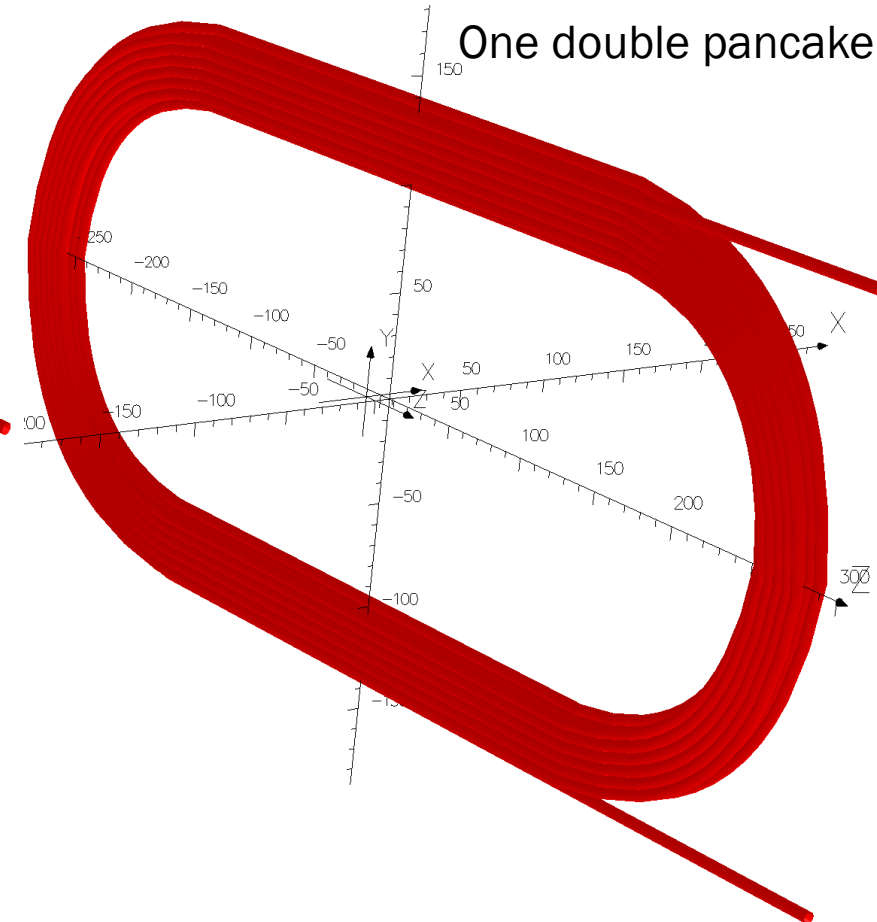


## 3-d modeling of the 6&8 turn CORC Coil (with 20 node BRICK in OPERA3d)

Two double pancakes



One double pancake



Modeling includes, leads  
and transition regions





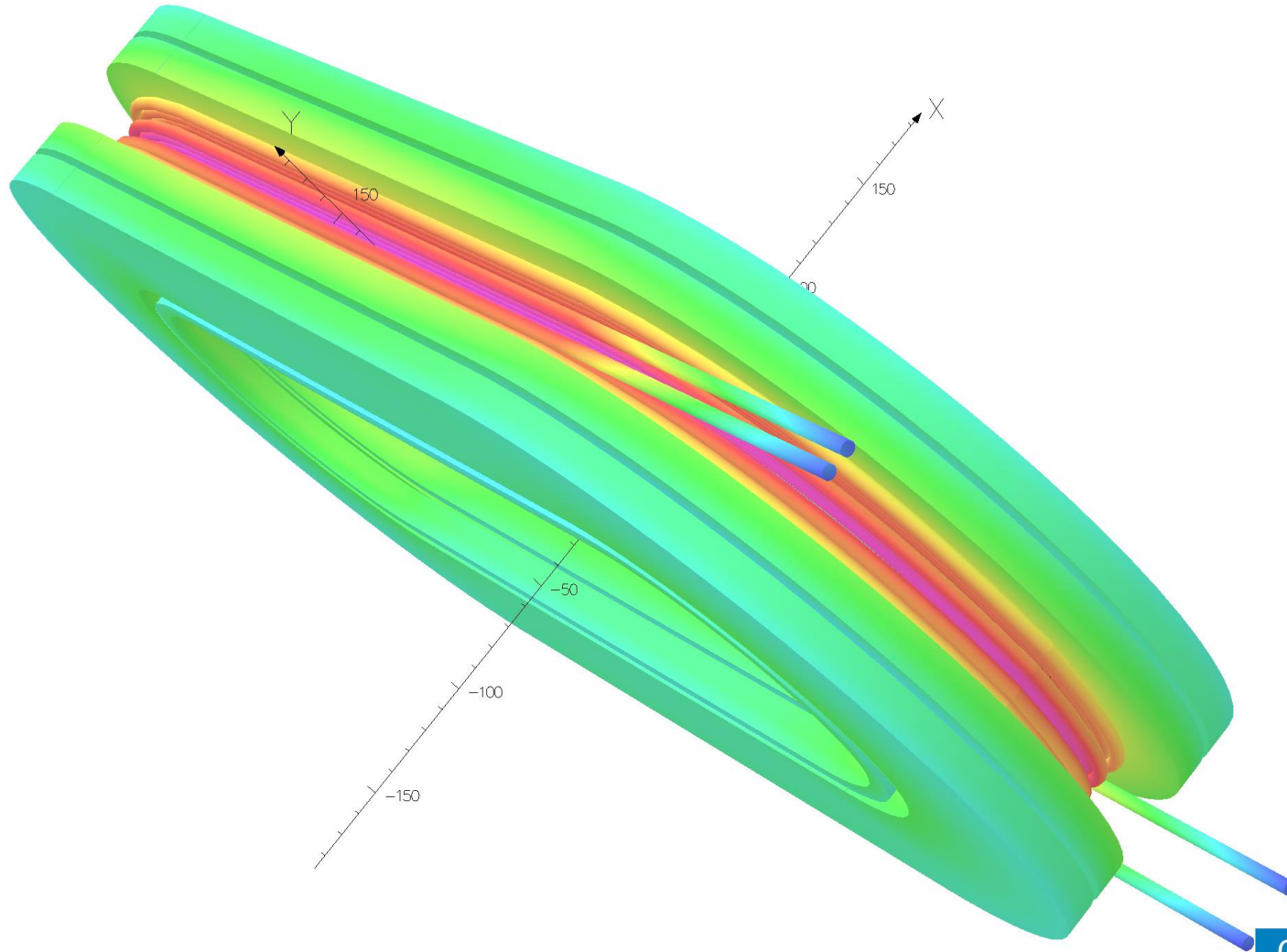
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# Field on the Hybrid coils at 10 kA (1) (6 & 8 turn CORC cable coil with Nb<sub>3</sub>coils)

3/June/2019 13:29:30

Surface contours: B

1.185009E+001  
1.000000E+001  
8.000000E+000  
6.000000E+000  
4.000000E+000  
2.000000E+000  
7.956284E-001



UNITS  
Length: mm  
Magn Flux Density: T  
Magn Field: A m<sup>-1</sup>  
Magn Scalar Pot: A  
Magn Vector Pot: Vb m<sup>-1</sup>  
Elec Flux Density: C m<sup>-2</sup>  
Elec Field: V m<sup>-1</sup>  
Conductivity: S m<sup>-1</sup>  
Current Density: A mm<sup>-2</sup>  
Power: W  
Force: N  
Energy: J  
Mass: kg

MODEL DATA  
66 conductors

Field Point Local Coordinates  
Local = Global

Opera



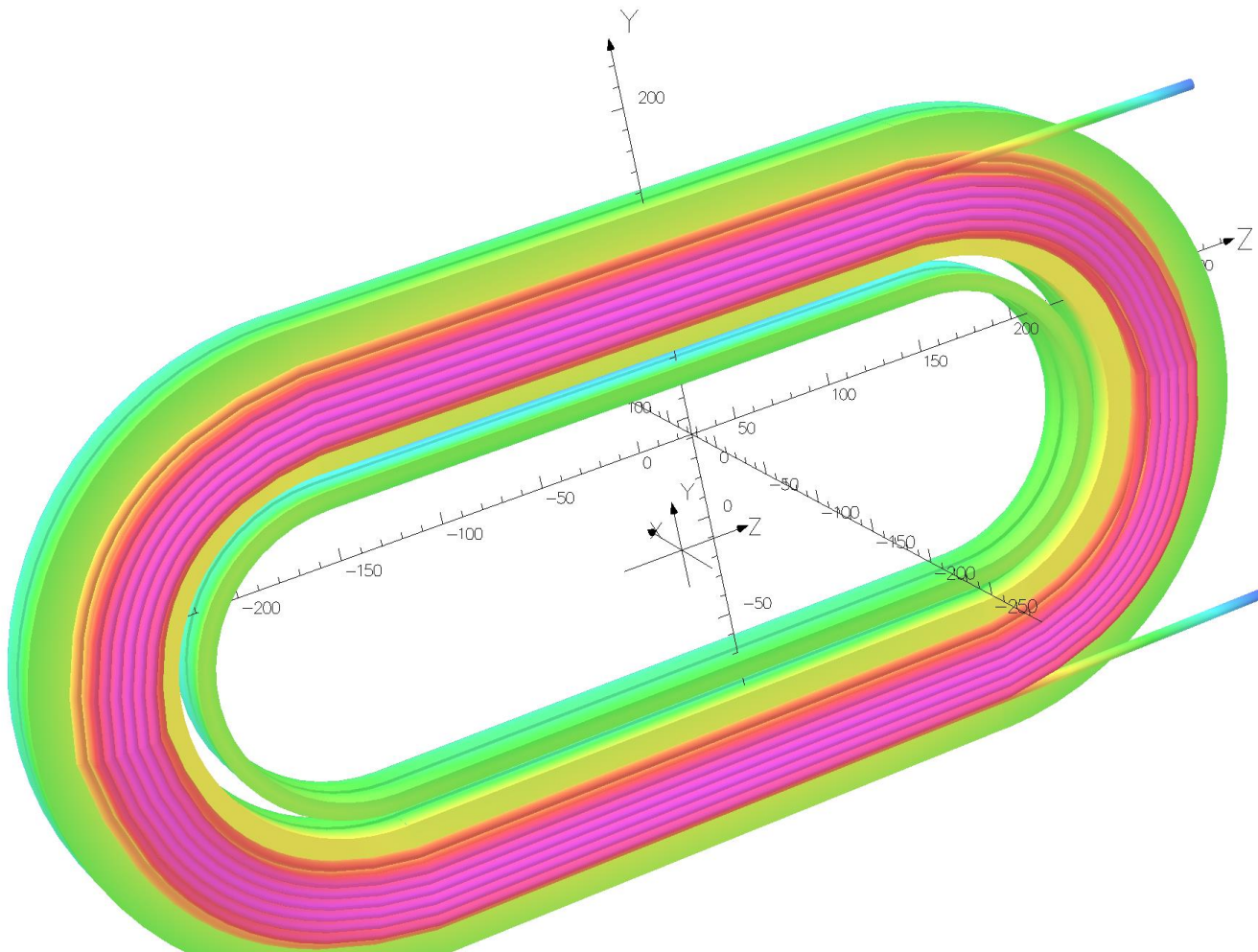
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**ENERGY** | Office of  
Science

# Field on the Hybrid coils at 10 kA (2) (6 & 8 turn CORC cable coil with Nb<sub>3</sub>coils)

3/Jun/2019 12:56:47

Surface contours: B

1.185009E+001  
1.000000E+001  
8.000000E+000  
6.000000E+000  
4.000000E+000  
2.000000E+000  
7.956284E-001



UNITS  
Length mm  
Magn Flux Density T  
Magn Field A m<sup>-1</sup>  
Magn Scalar Pot A  
Magn Vector Pot Vb m<sup>-1</sup>  
Elec Flux Density C m<sup>-2</sup>  
Elec Field V m<sup>-1</sup>  
Conductivity S m<sup>-1</sup>  
Current Density A mm<sup>-2</sup>  
Power W  
Force N  
Energy J  
Mass kg

MODEL DATA  
66 conductors

Field Point Local Coordinates  
Local = Global

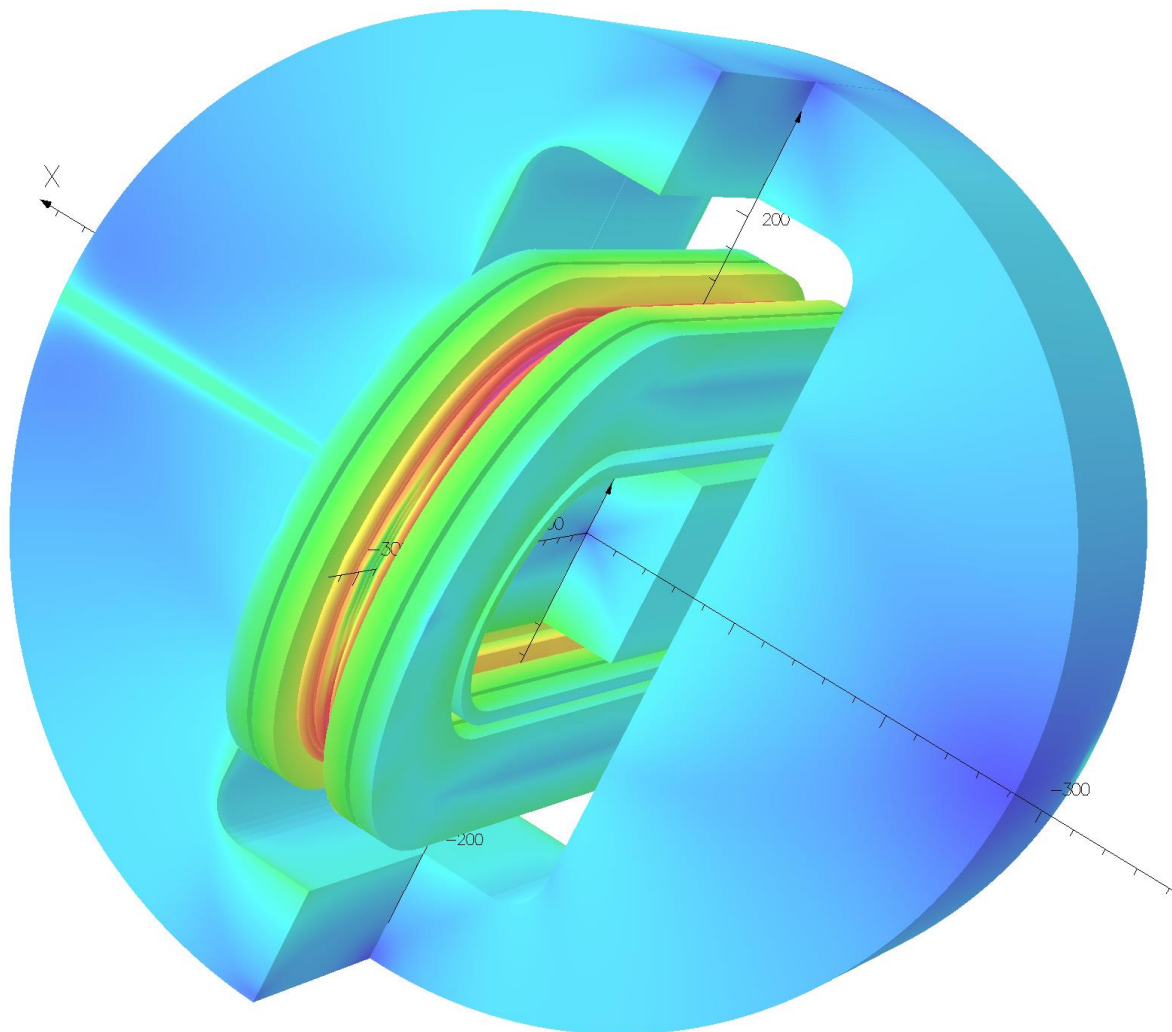
Opera

# Hybrid Magnet Model with Iron

3Jun2019 08:17:00

Surface contours: B

1.255861E+001  
1.200000E+001  
1.000000E+001  
8.000000E+000  
6.000000E+000  
4.000000E+000  
2.000000E+000  
6.980407E-003



## UNITS

Length mm  
Magn Flux Density T  
Magn Field A m<sup>-1</sup>  
Magn Scalar Pot A  
Magn Vector Pot Wb m<sup>-1</sup>  
Elec Flux Density C m<sup>-1</sup>  
Elec Field V m<sup>-1</sup>  
Conductivity S m<sup>-1</sup>  
Current Density A mm<sup>2</sup>  
Power W  
Force N  
Energy J  
Mass kg

## MODEL DATA

com-cor-c-collab-y118-6-8turns.ap3  
TOSCA Magnetostatic  
Nonlinear materials  
Simulation No 1 of 1  
47840 elements  
494593 nodes  
66 conductors

Nodally interpolated fields  
Activated in global coordinates  
Reflection in XY plane (Z field=0)  
Reflection in YZ plane (X field=0)  
Reflection in ZX plane (Y field=0)

## Field Point Local Coordinates

Local = Global

## FIELD EVALUATIONS

Line LINE (nodes) 101 Cartesian  
x=-50.0 to 50.0 y=90.0 z=0.0

Opera



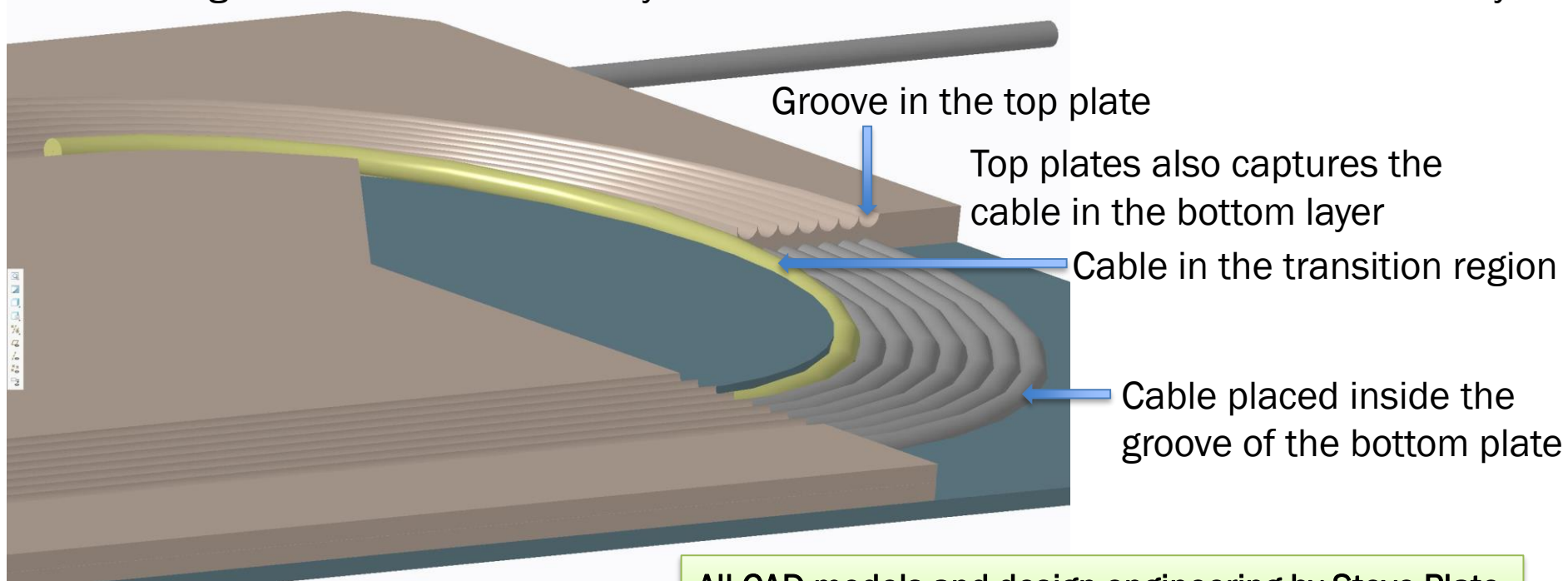
# Coil Winding and the Mechanical Structure

- BNL and ACT are working together on developing the coil winding techniques and on the mechanical structure.
- BNL task in STTR is to help ACT with the design, etc.. ACT will purchase the parts and wind the coil (limited budget of STTR precluded BNL to actually wind the coils).
- BNL will design, purchase all parts and wind the coil for MDP with the ACT supplied cable.
- This presentation will include the initial BNL design geared for efficiency and providing mechanical support to individual cable.
- As such major forces on the CORC cable are in horizontal direction but vertical forces also become significant on certain turns.



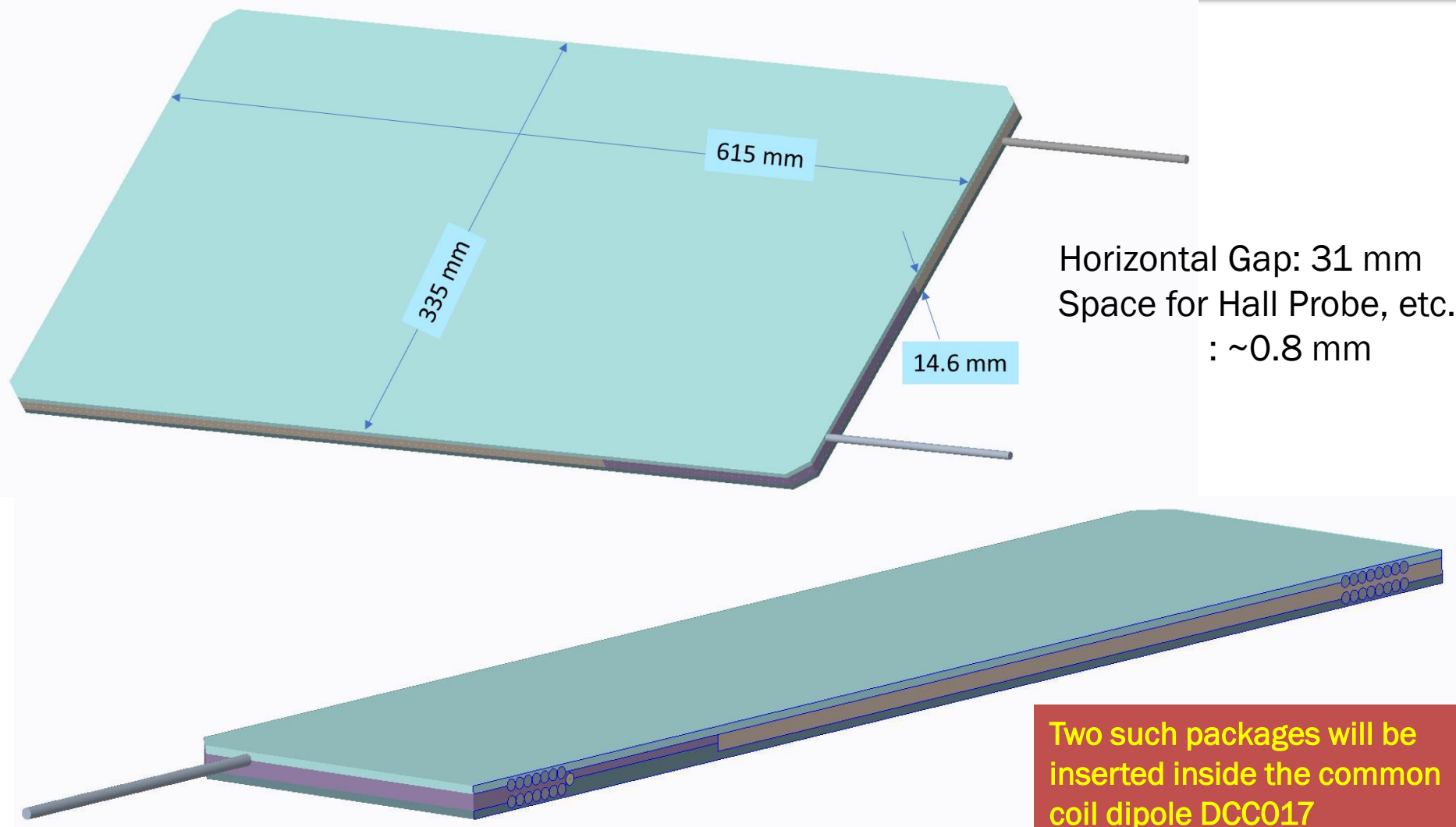
# The Basic Design Concept

The conductor is placed inside the grooves machined in the SS plates (or 3-d printed). Each turn is fully captured (with thin epoxy) and thus fully supported. We may need to work with the cable to place it in the grooves. Major component of the Lorentz force is horizontal which can be taken by the thickness of the plate, as and if needed (as such CORC coil lean on  $\text{Nb}_3\text{Sn}$  coils). Small component of the vertical Lorentz force can be taken by the structure between the groove. The two turns nearly touch each other for the maximum current density.



All CAD models and design engineering by Steve Plate

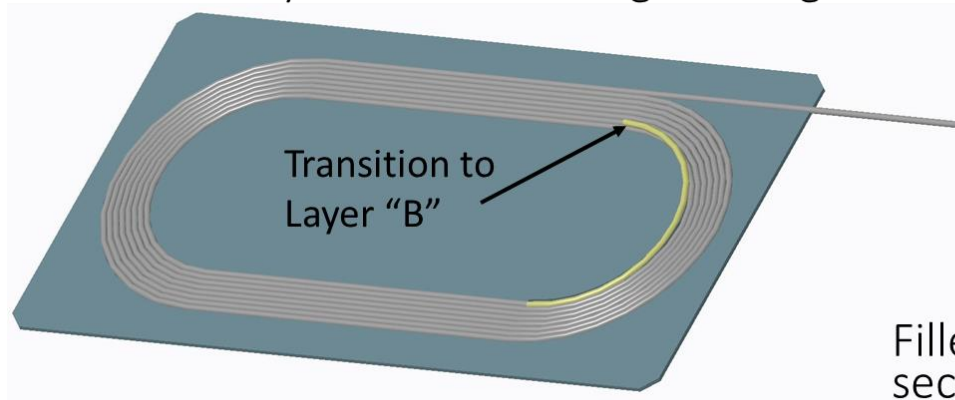
# Overall Design of a Double Pancake Package



# Key Coil Winding Steps (1)

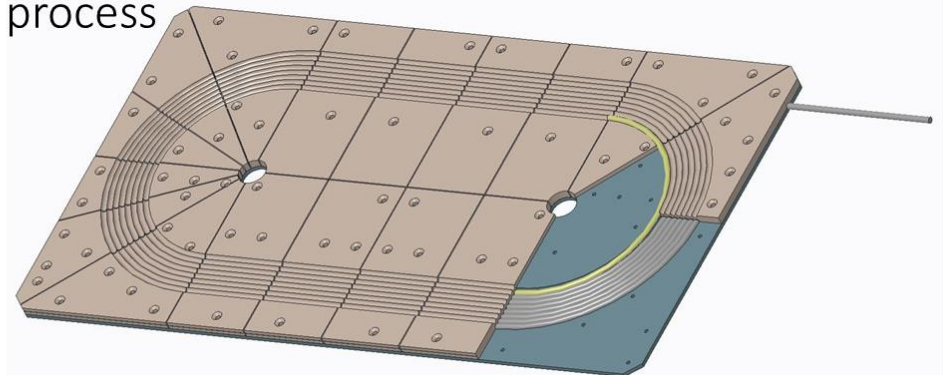
## Layer “A”

Paint track with epoxy, then wind CORC.  
Install Interlayer Filler #1 during winding.



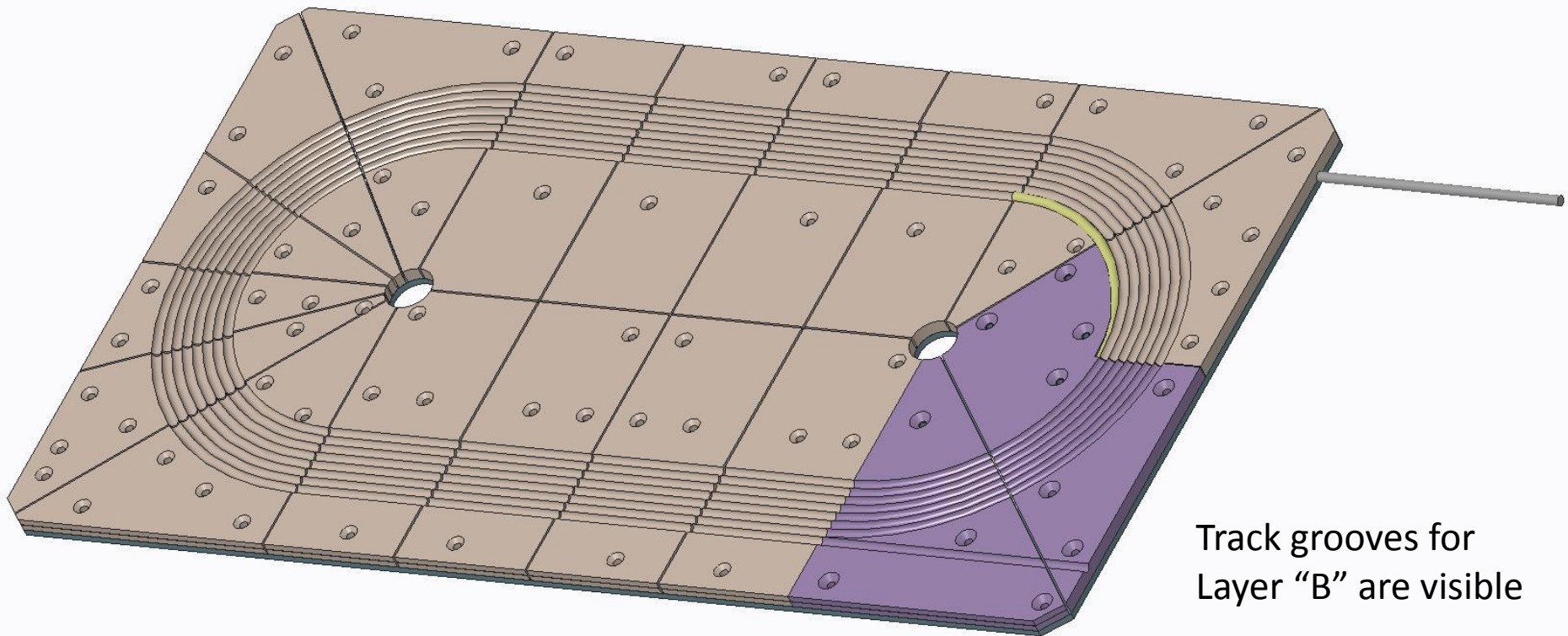
Conductor is continuous on spool, but not shown beyond transition

Filler #1 is segmented to allow individual sector installation and removal during winding process



# Key Coil Winding Steps (2)

Fully enclose Layer “A” by installing Filler #2

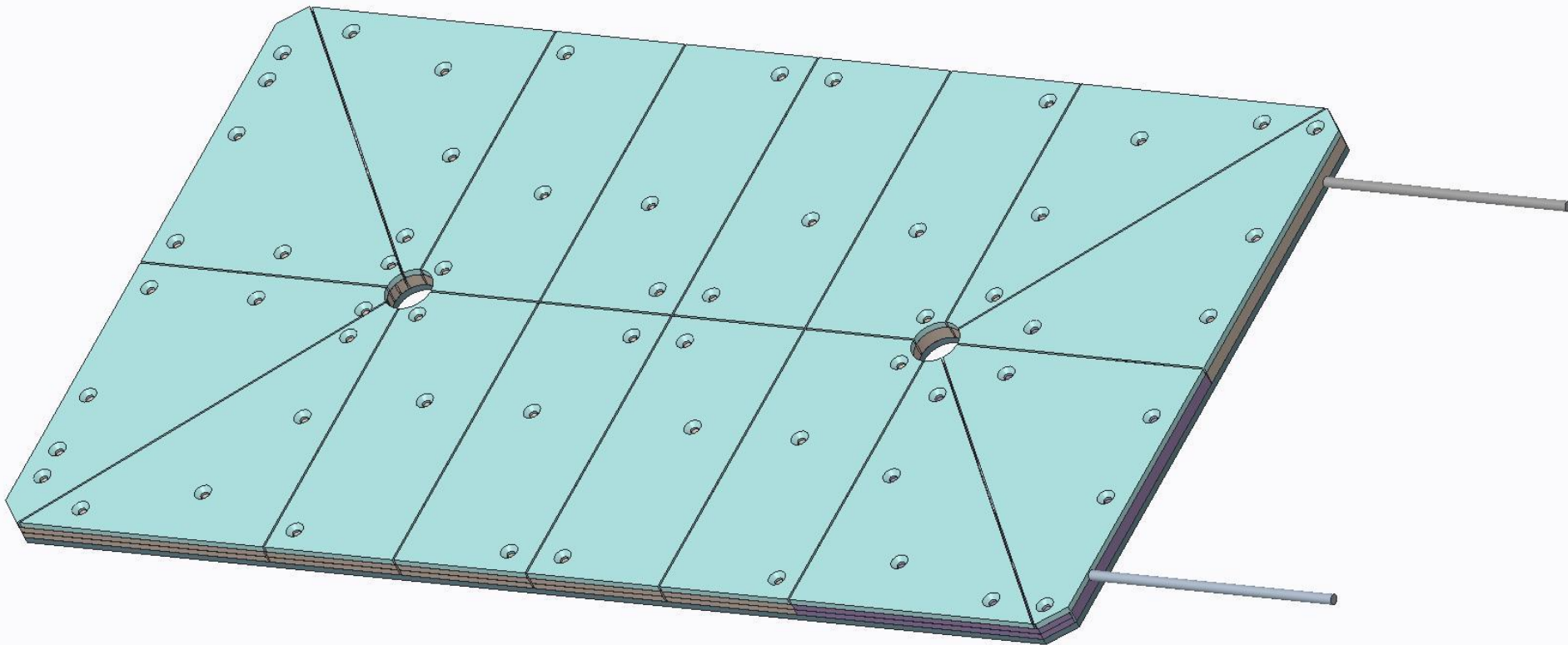


Track grooves for  
Layer “B” are visible



# Key Coil Winding Steps (3)

Segmented Track “B” clamps coil



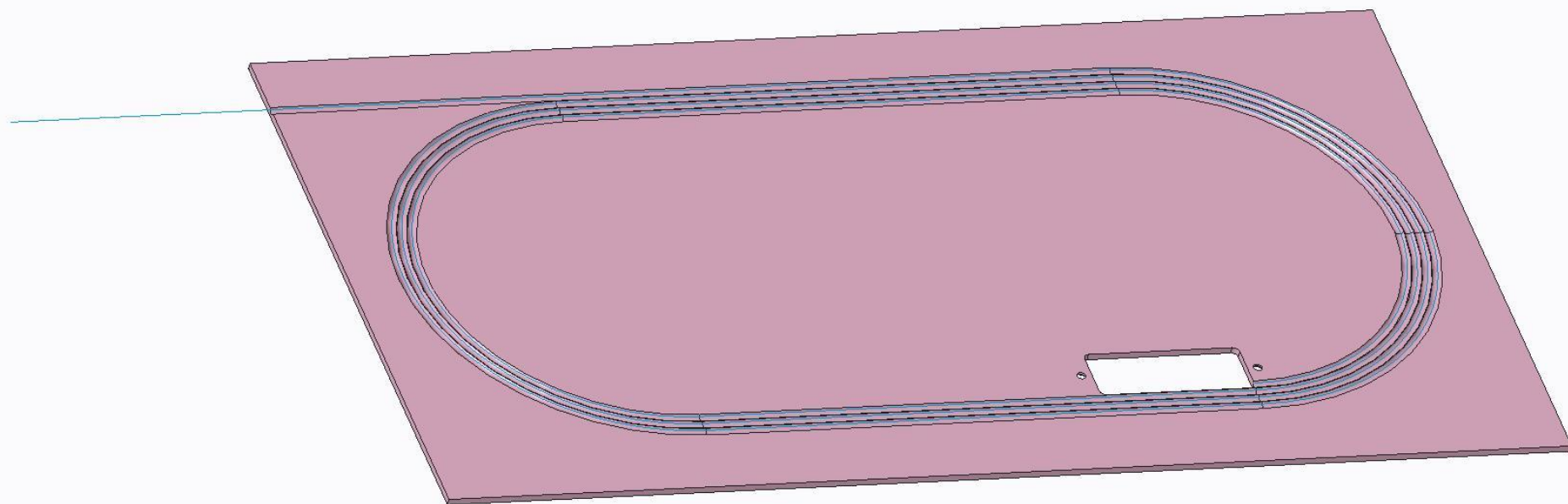


## CORC Coil for MDP

- As mentioned earlier, the CORC coil for MDP will have a total 8 turns ( $4 + 4$ ), instead of 28 in the STTR coil.
- A significant amount of cable ( $\sim 13$  meters) for quench studies.
- There are three options for designing and placing this insert coil:
  1. Two 4 turns form a double pancake with S-transition to reverse the direction of current with  $\sim 15$  mm gap for instrumentation.
  2. Small gap in the middle but more gap and support structure on either side.
  3. A double pancake making contact to the Nb<sub>3</sub>Sn coils on one side and gap on the other side.

The baseline design is option #1. But we may evaluate others as well.

## Step 1: Base Track for Layer “A”

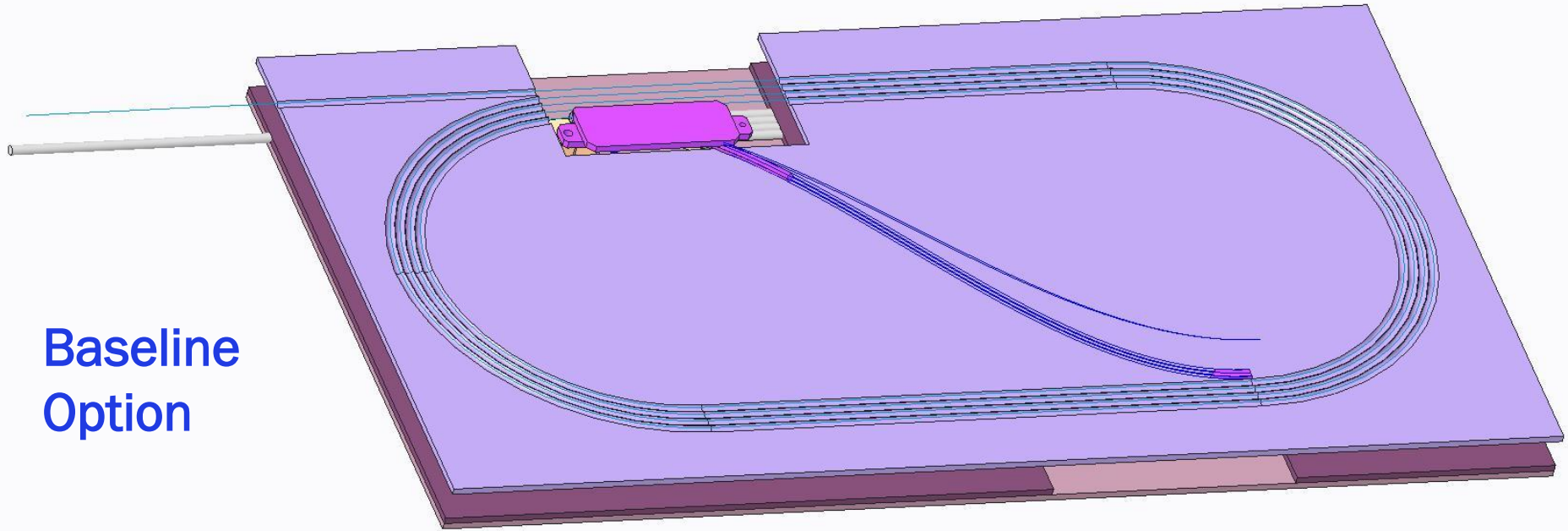




# Special 4-turn Double Pancake Coil in support Structure

(current in the 2 pancakes in opposite direction and a gap in between)

## Step 5: Install Base Track for Layer “B”



Baseline  
Option

S-turn in transition region changes the direction of the current between the two pancakes.  
It should tolerate some horizontal motion (as was the case for the splice during the last test).



# Initial Discussions (1)

## (Notes from Xiaorong Wang)

- Powering scheme
  - Baseline: the CORC<sup>®</sup> coil will be connected in series with the power supply for the Nb<sub>3</sub>Sn magnet up to 10 kA.
  - BNL is working to set up a 17 kA power supply to power the CORC<sup>®</sup> coil separately.
- Driving questions for the quench experiments
  - Can we study the transition behavior of the coil with the series-powering scheme? [see required information below] If yes, how does the coil transition in 10 T background field? Is the transition smooth with the capability to ramp the current up and down along the transition?
  - Considering the margin of the CORC<sup>®</sup> coil at various fields, can we induce a quench with a heater? What is the total power generated by the heater to induce a quench at various background fields? Does the normal zone propagate during a quench at various background fields? Can we measure the propagation velocity?
  - How does current distribute between tapes at the front of growing normal zone?
  - Can we detect the local temperature rise due to the heater with different instrumentations such as acoustic and fiber-optic sensors? How does different instrumentations compare with each other?

# Initial Discussions (2)

## (Notes from Xiaorong Wang)

- With the fiber-optic sensor, can we tell if the coil starts the transition in the peak field region?
- Does the transition current of the CORC<sup>®</sup> coil depend on the number of ramping? Any impact of the current/Lorentz force cycling? Similarly, does the quench energy reduce after cycling? Does the normal zone propagates faster after cycling? Does the current sharing behavior change after cycling? Does the transition current of the CORC<sup>®</sup> coil depend on the ramp rate?
- Can we probe the MIITs limit for the CORC<sup>®</sup> coil at 10 T? This can potentially degrade the CORC<sup>®</sup> coil and should be performed toward the end of the test campaign.
- Information needed to design the experiments and plan the required instrumentation:
  - Coil design or dimensions to determine locations of potential instrumentation
  - Predicted short-sample performance for the CORC<sup>®</sup> coil at 4.2 K, different fields up to 10 T. The peak field region in the CORC<sup>®</sup> coil and the fields at other specific locations. This information can help to optimize the location(s) of the spot heater(s).

# Initial Discussions (3)

## (Notes from Xiaorong Wang)

- Desired instrumentation:
    - Acoustic sensors to detect temperature rise and quench (coordinate with Maxim)
    - Hall sensor array to detect local current sharing between tapes and propagation of normal zone (Maxim)
    - Fiber optic sensor to measure temperature profile along the conductor (coordinate with Justin)
    - Voltage taps in the conductor terminal (installed by ACT or during coil fabrication)
- At this initial stage, we need to do high level planning in terms of evaluating what we want to do, what is technically important, what can be done with the resources we have, what space is needed to do various experiments, what groups involved in planning, etc. ,...
  - For most of this we need to have a separate smaller group working meeting. We should do that soon, perhaps about now.

# Summary and Conclusions

- **Our initial thinking on the ReBCO based R&D program for USMDP has been laid out. We welcome input from collaboration.**
- **Common coil dipole DCC017 has been designed as a test facility magnet. We would like this R&D to progress with that philosophy.**
- **Please let us know if you would like to join and we would include you in smaller group discussions.**
- **Task #1 is primarily for magnetization studies but other components can be included as long as it fits with the resources.**
- **Task#2 for quench studies has been just started. We need significant planning, etc.**





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Extra Slides

