



U.S. MAGNET
DEVELOPMENT
PROGRAM

20 T HTS/LTS Hybrid Common Coil Design

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August 24, 2021



U.S. DEPARTMENT OF
ENERGY

Office of
Science

20T HTS/LTS Hybrid Common Coil Design

-Ramesh Gupta, BNL

August 24, 2021

A reasonably evolved HTS/LTS Hybrid Common Coil Design

- **Optimized for a good field quality**
- **Provides desired margin even at 4 K in both HTS and Nb₃Sn**
- **Space for managed structure included**
 - **To be verified by the actual mechanical analysis**
 - **A conceptual structure for CORC shown; other possibilities**
- **Common coil design allows higher J_e or J_o CORC**
- **Same magnetic design is used for both CORC and Bi2212**

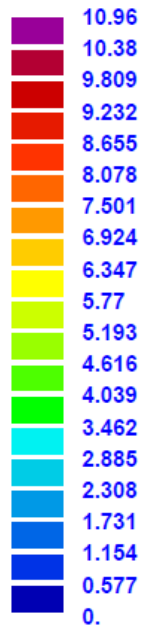


50 mm, 20 T Common Coil Hybrid Design

MDP 20T Hybrid CORC/Bi2212 + Nb3Sn Common Coil Dipole

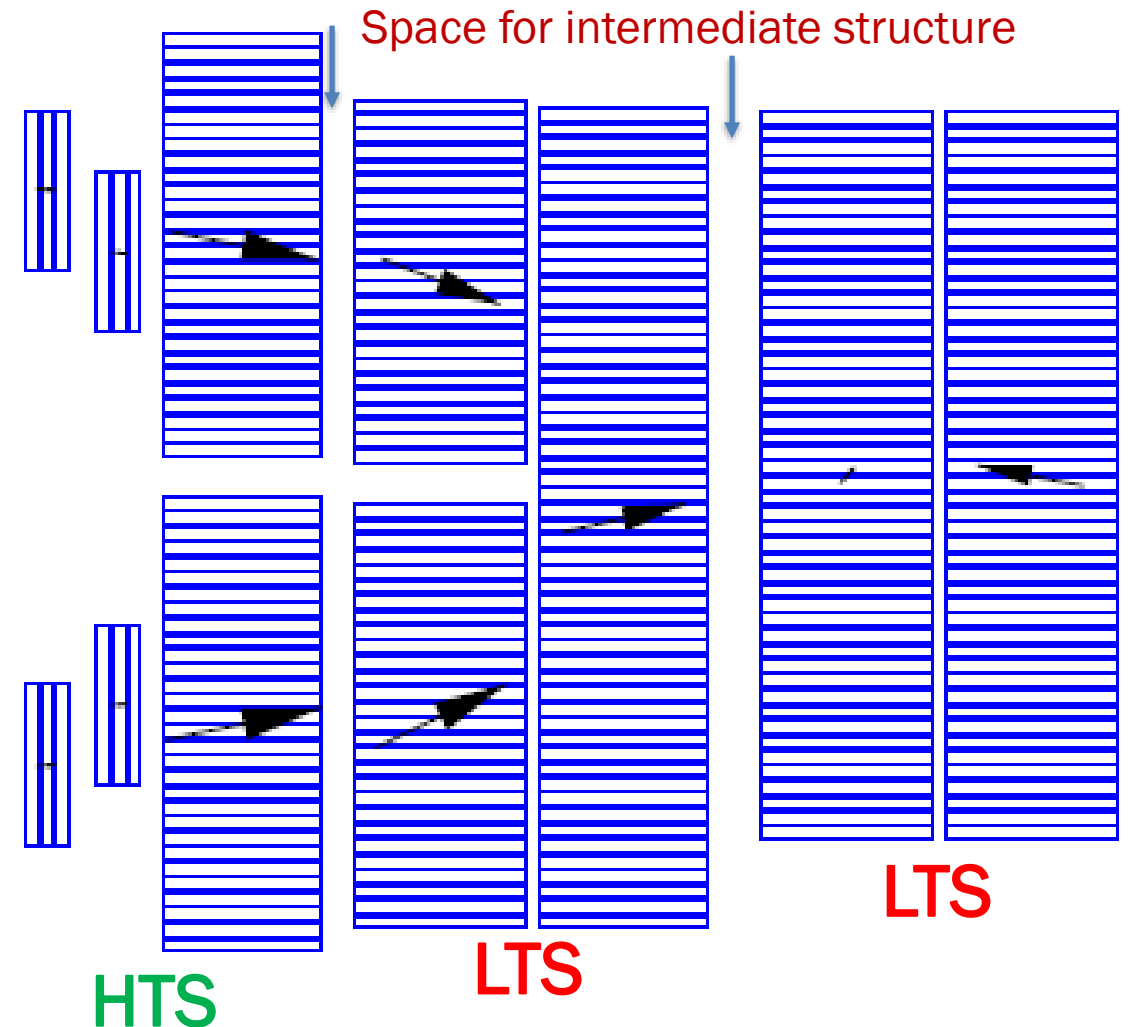
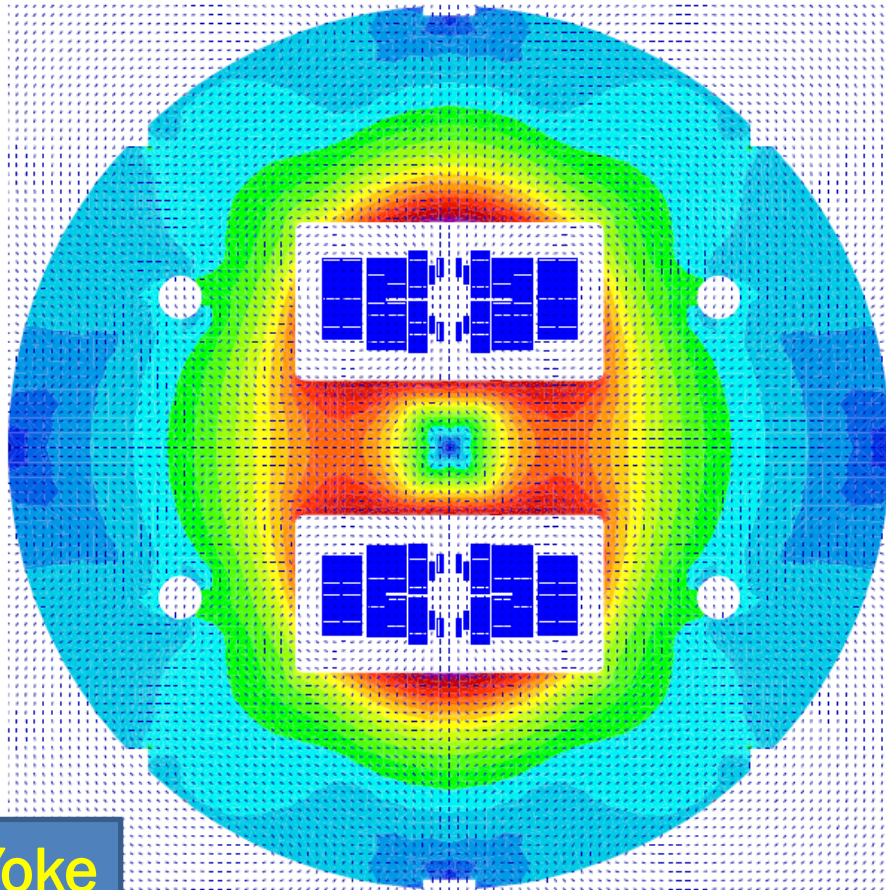
21/08/23 08:56

|B| flux density (T)



ROXIE 10.2

Field in Yoke



Field Quality in 20 T Common Coil Hybrid Design

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HARMONIC ANALYSIS NUMBER ..... 1
MAIN HARMONIC ..... 1
REFERENCE RADIUS (mm) ..... 15.0000
X-POSITION OF THE HARMONIC COIL (mm) ..... 0.0000
Y-POSITION OF THE HARMONIC COIL (mm) ..... 169.0000
MEASUREMENT TYPE ..... ALL FIELD CONTRIBUTIONS
ERROR OF HARMONIC ANALYSIS OF Br ..... 0.2915E-03
SUM (Br(p) - SUM (An cos(np) + Bn sin(np))

MAIN FIELD (T) ..... 20.097535
MAGNET STRENGTH (T/ (m^(n-1)) ..... 20.0975
  
```

**All harmonics
<10⁻⁴**

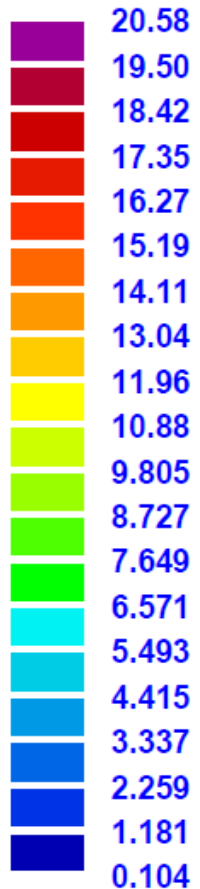
*** Mostly 10⁻⁵ ***

NORMAL RELATIVE MULTIPOLES (1.D-4):						SKEW RELATIVE MULTIPOLES (1.D-4):					
b 1:	10000.00000	b 2:	0.00000	b 3:	0.00886	a 1:	0.00000	a 2:	0.01125	a 3:	0.00000
b 4:	0.00000	b 5:	0.00866	b 6:	-0.00000	a 4:	0.02070	a 5:	-0.00000	a 6:	0.09133
b 7:	-0.12569	b 8:	0.00000	b 9:	-0.14757	a 7:	0.00000	a 8:	-0.18568	a 9:	-0.00000
b10:	0.00000	b11:	-0.25870	b12:	-0.00000	a10:	-0.32507	a11:	-0.00000	a12:	-0.10123
b13:	-0.09200	b14:	0.00000	b15:	0.01722	a13:	0.00000	a14:	0.02355	a15:	-0.00000
b16:	0.00000	b17:	0.00085	b18:	-0.00000	a16:	-0.00354	a17:	-0.00000	a18:	-0.00405



50 mm, 20 T Common Coil Hybrid Design

$|B|$ (T)



$B_0 = 20.1\text{T}$

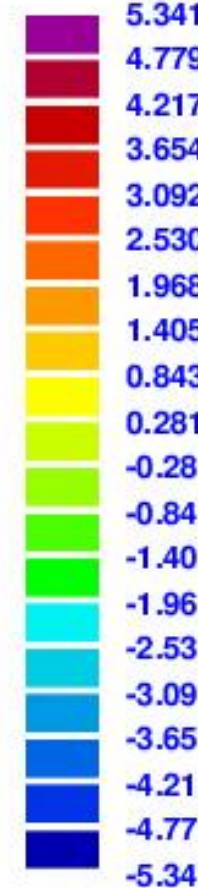
HTS

LTS

LTS

**Peak Enhancement
~2.4%**
(low peak field enhancement)

J (A/mm²)



HTS

LTS

LTS

J_{overall}
325 A/mm²

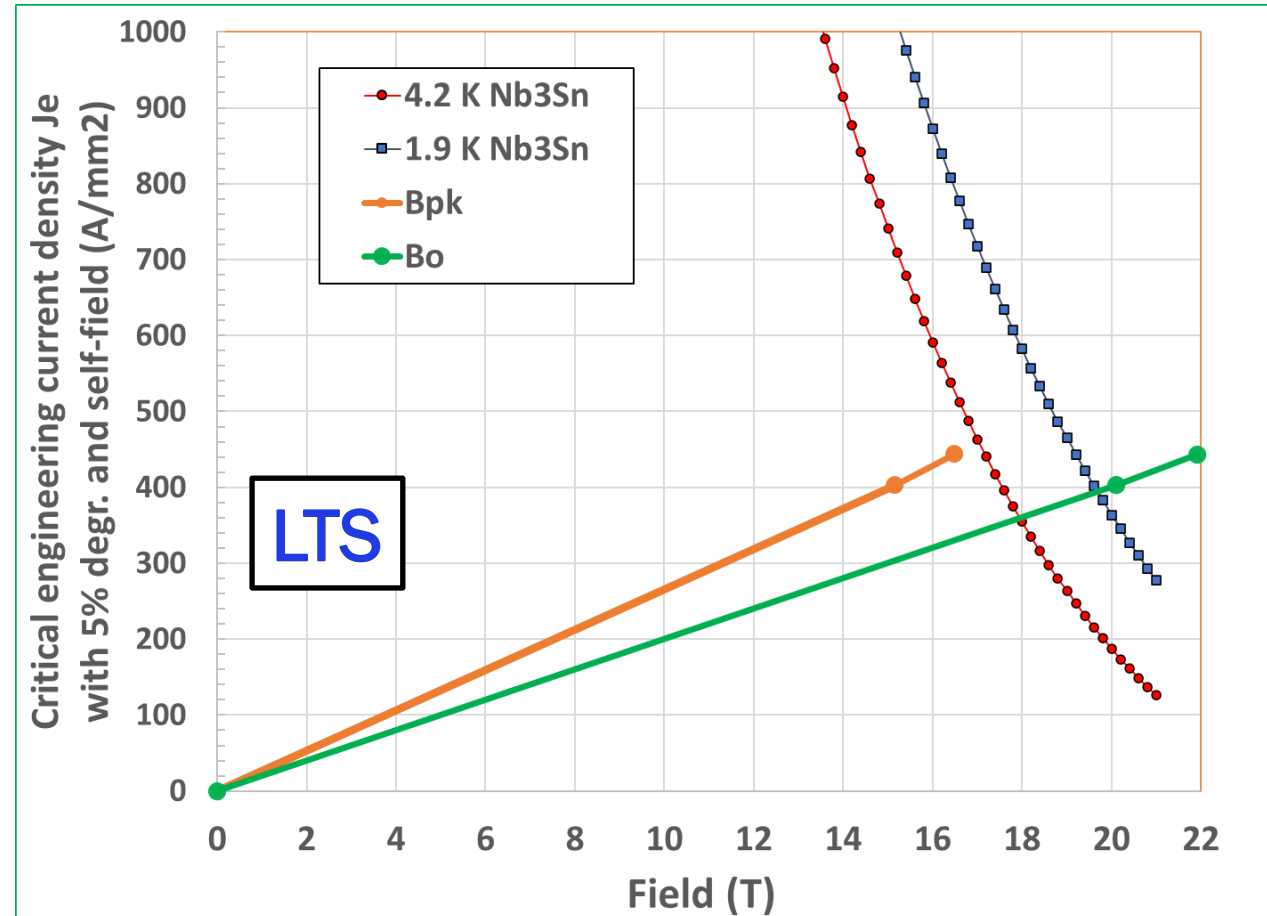
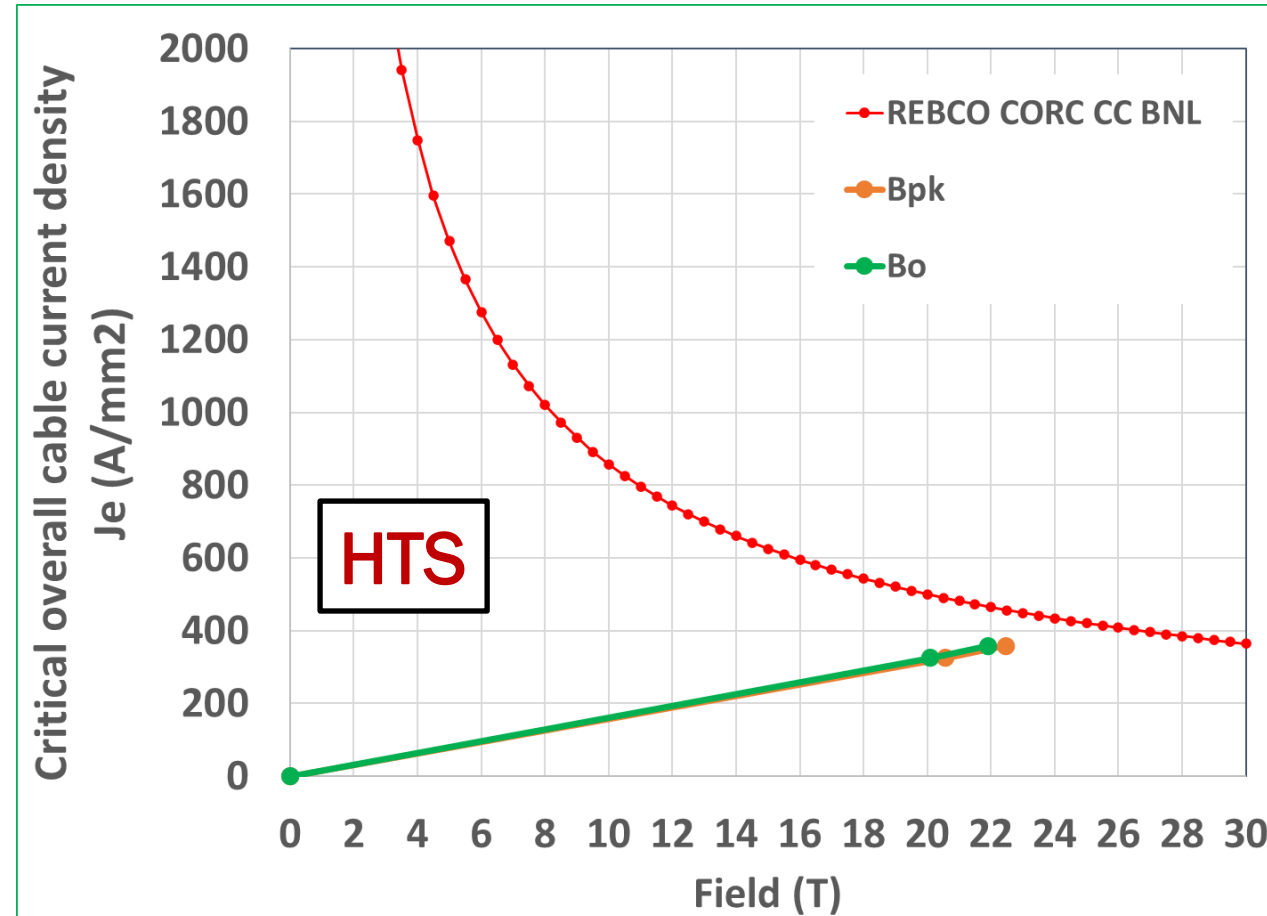
J_{overall}
403 A/mm²

J_{overall}
403 A/mm²

J_0 same as in Vittorio's Bi2212 design
 J_0 in CORC for Common Coil can be higher

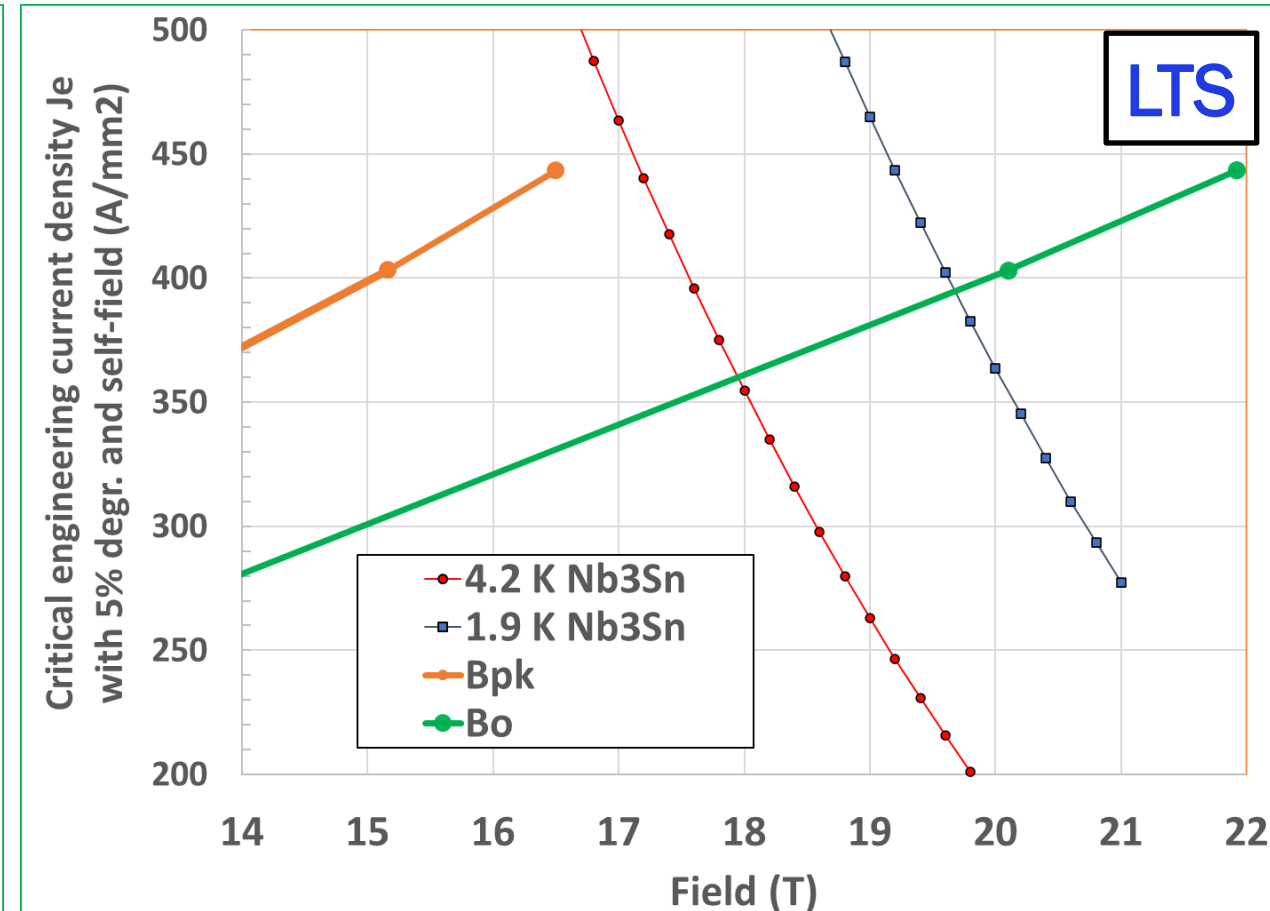
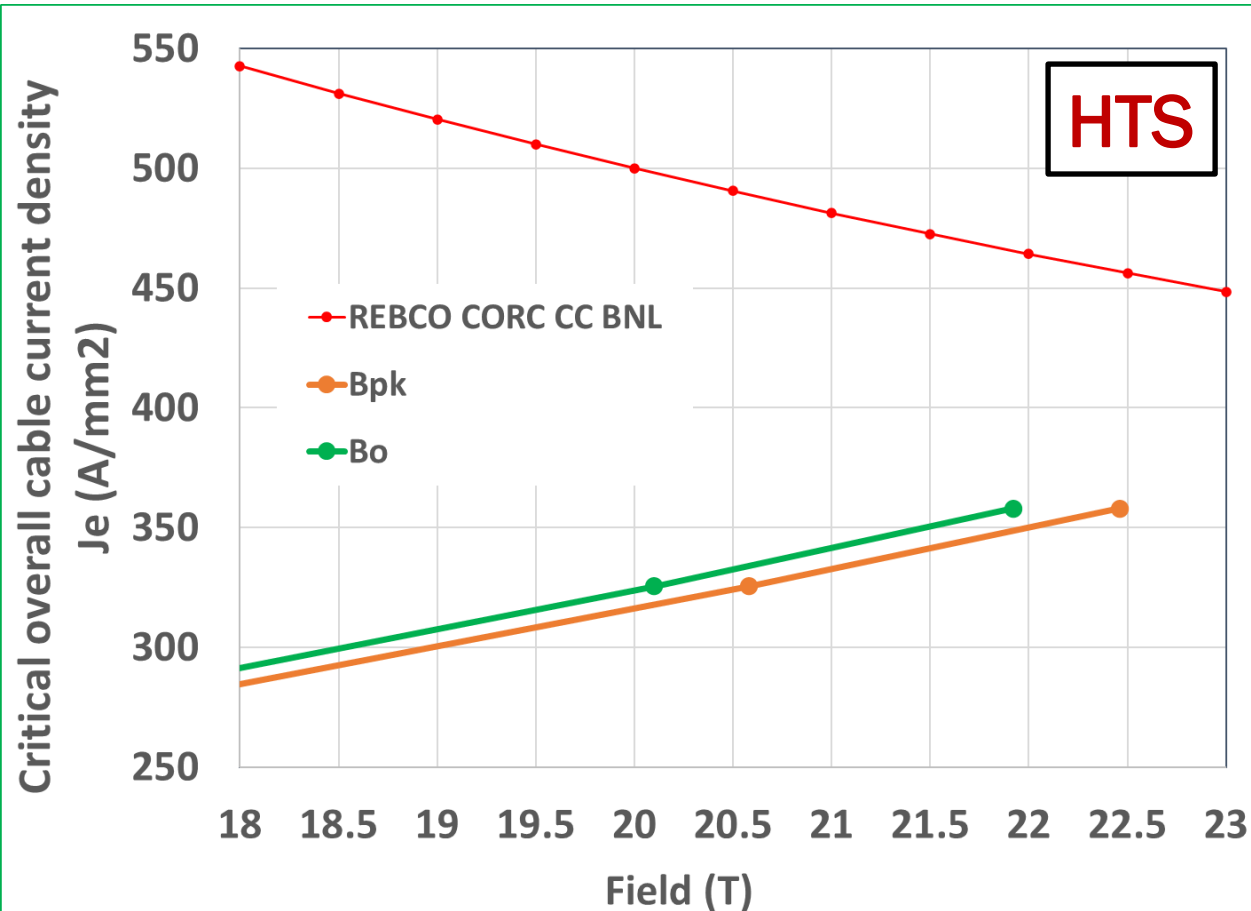
Margins in 20 T Hybrid Common Coil Design

➤ Enough margin at 4.2 K as well



Margins in 20 T Hybrid Common Coil Design

➤ Enough margin at 4.2 K as well



Conductor Used (1)

HTS (Bi2212 or CORC)

NUMBER OF BLOCK	1
NUMBER OF CONDUCTORS	3
POSITIONING ANGLE (DEG)	214.4000
INCLINATION ANGLE (DEG)	-90.0000
CURRENT IN EACH CONDUCTOR OF THE BLOCK (A)	-12500.0000
INNER RADIUS OF THE BLOCK (MM)	18.1636
CABLE HEIGHT (MM) . (INSULATED)	20.2594
CABLE INNER WIDTH (MM) . (INSULATED)	1.8962
CABLE OUTER WIDTH (MM) . (INSULATED)	1.8962
CABLE HEIGHT (MM) . (BARE)	19.9600
CABLE INNER WIDTH (MM) . (BARE)	1.5968
CABLE OUTER WIDTH (MM) . (BARE)	1.5968
RADIAL INSULATION THICKNESS (MM)	0.1497
AZIMUTHAL INSULATION THICKNESS (MM)	0.1497
NUMBER OF STRANDS	50
DIAMETER OF STRANDS (MM)	0.8000
CU/SC RATIO	3.0000
RESIDUAL RESISTIVITY RATIO	100.0000
TEMPERATURE AT WHICH JC AND DJC ARE GIVEN (K)	1.9000
LINEAR APPROXIMATION JC (20.0 T) (A/MM**2)	2944.000
LINEAR APPROXIMATION DJC/DB (A/MM**2 T)	64.000
CABLING ANGLE (DEG)	1.373
NUMBER OF DISCRETISATION POINTS AZIMUTHAL	2
NUMBER OF DISCRETISATION POINTS RADIAL	10
CONDUCTOR NAME	MDPB2212

Nb₃Sn

NUMBER OF BLOCK	5
NUMBER OF CONDUCTORS	28
POSITIONING ANGLE (DEG)	110.0000
INCLINATION ANGLE (DEG)	0.0000
CURRENT IN EACH CONDUCTOR OF THE BLOCK (A)	-16500.0000
INNER RADIUS OF THE BLOCK (MM)	48.9020
CABLE HEIGHT (MM) . (INSULATED)	21.5867
CABLE INNER WIDTH (MM) . (INSULATED)	1.8962
CABLE OUTER WIDTH (MM) . (INSULATED)	1.8962
CABLE HEIGHT (MM) . (BARE)	21.2873
CABLE INNER WIDTH (MM) . (BARE)	1.5968
CABLE OUTER WIDTH (MM) . (BARE)	1.5968
RADIAL INSULATION THICKNESS (MM)	0.1497
AZIMUTHAL INSULATION THICKNESS (MM)	0.1497
NUMBER OF STRANDS	55
DIAMETER OF STRANDS (MM)	0.8000
CU/SC RATIO	1.0000
RESIDUAL RESISTIVITY RATIO	100.0000
TEMPERATURE AT WHICH JC AND DJC ARE GIVEN (K)	1.9000
LINEAR APPROXIMATION JC (16.0 T) (A/MM**2)	1928.000
LINEAR APPROXIMATION DJC/DB (A/MM**2 T)	371.000
CABLING ANGLE (DEG)	1.361
NUMBER OF DISCRETISATION POINTS AZIMUTHAL	2
NUMBER OF DISCRETISATION POINTS RADIAL	10
CONDUCTOR NAME	MDPH1

Conductor Used (2)

Edit Cable Data [/home/gupta/MDP/2021/roxie_mdp-aug-2021-cc.cadata]

File Display

Cable Definition

No	Name	Cable Geom.	Strand	Filament	Insul	Trans	Quench Mat.	T ₀	Comment
41	MDPW1	MDPW1	MDPWJC	NB3SN	MDPW1	NONE	NONE	1.9	MDP
42	MDPW2	MDPW2	MDPWJC	NB3SN	MDPW1	NONE	NONE	1.9	MDP
43	MDPH1	MDPW1	MDPHJC	ECC2	MDPW1	NONE	NONE	1.9	MDP
44	MDPH2	MDPW2	MDPHJC	ECC2	MDPW1	NONE	NONE	1.9	MDP
45	MDPB2212	MDPB2212	MDPW2212	NB3SN	MDPW1	NONE	NONE	1.9	MDP
46	MDPCCCORC	MDPCCCORC	MDPCCCORC	NB3SN	MDPW1	NONE	NONE	1.9	MDP Common Coil CORC

Edit Cable Data [/home/gupta/MDP/2021/roxie_mdp-aug-2021-cc.cadata]

File Display

Transient

Quench Material Properties

Cable Geometry

No	Name	height	width_i	width_o	ns	transp.	degrd	Comment
42	MDPW1	21.33	1.6	1.6	55	100	0	MDP NB3SN
43	MDPW2	13.3	1.6	1.6	37	100	0	MDP NB3SN
44	MDPB2212	20	1.6	1.6	50	100	0	MDP Bi2212
45	MDPCCCORC	20	1.6	1.6	50	100	0	MDP Common Coil CORC

File Display

Filament

Strand

No	Name	diam.	cu/sc	RRR	Tref	Bref	Jc@BrTr	dJc/dB
20	MDPWJC	0.8	1	100	1.9	16	1928	371
21	MDPHJC	0.8	1	100	1.9	16	1928	371
22	MDP2JC	1.1	1	100	1.9	16	1928	371
23	MDPW2212	0.8	3	100	1.9	20	2944	64
23	MDPCCCORC	0.8	3	100	1.9	20	2944	64

Edit Cable Data [/home/gupta/MDP/2021/roxie_mdp-aug-2021-cc.cadata]

File Display

Filament

No	Name	fildiao	fildiai	Jc-Fit	Comment
4	NBTIO	6	0	FIT1	NBTI OUTER CABLES
5	NB3SN	22	12	FIT1	NB2SN TWENTE
6	NBTIS	5	0	FIT1	NBTI SIEMAT(ALSTOM)
7	NBTIG	6	0	GSIFIT	NBTI GSI001
8	SIS3NBTI	3.5	0	SISFIT	NBTI SIS300
9	NB3AL	50	0	NBALK1	Nb3Al tes
10	NB3SNI	10	0	FIT1	ITER RF
11	EUNB3SN	30	0	EUFIT1	EUROCOIL NB3SN
12	ECC2	50	0	ECCB2	NB3SN FCC 2300 A/mm ²

Edit Cable Data [/home/gupta/MDP/2021/roxie_mdp-aug-2021-cc.cadata]

File Display

Insulation

Jc-Fit

No	Name	Type	Jcref	Tc0	alpha	beta	gamma	C0	Bc20	N/a	N/a	N/a	N/a	Comment
1	FIT1	1	3E+09	9.2	0.57	0.9	2.32	27.04	14.5	0	0	0	0	0 MB FILAMENT TYPE
2	TES1	1	3E+09	9.2	0.57	0.9	2.32	27.04	14.5	0	0	0	0	0 FILAMENT TEST TYPE alph
3	GSIFIT	1	3E+09	9.2	0.7	1.57	1	25	14.5	0	0	0	0	0 APPROXIMATE THE WILSON
4	SISFIT	1	3E+09	9.33517	0.68	0.8477	2.23234	25	14.5	0	0	0	0	0 Glyn MQY15 FIT at 4.5K
5	NBALK1	5	1.4E+10	36.2	17.8	0	0	0	0	0	0	0	0	0 Jc fit of Nb3Al K1 at 4
6	EUFIT1	5	4.75E+10	28.9	18	0	0	0	0	0	0	0	0	0 EUROCOIL NB3SN FIT1
7	ECCB2	11	2.67845E+11	29.38	16	0.96	1.52	0.5	2	0	0	0	0	0 1350 A/MM ² AT 16 T 4.2

Insulation

No	Name	Radial	Azimut	Comment
24	MDPW1	0.15	0.15	MDP insulation
25	EUINS	0.15	0.15	EUROCOIL INSI

CORC in Common Coil

- STTR with ACT anticipated a future common coil CORC with an engineering current density of 600 A/mm²
- Checked with Danko – still possible

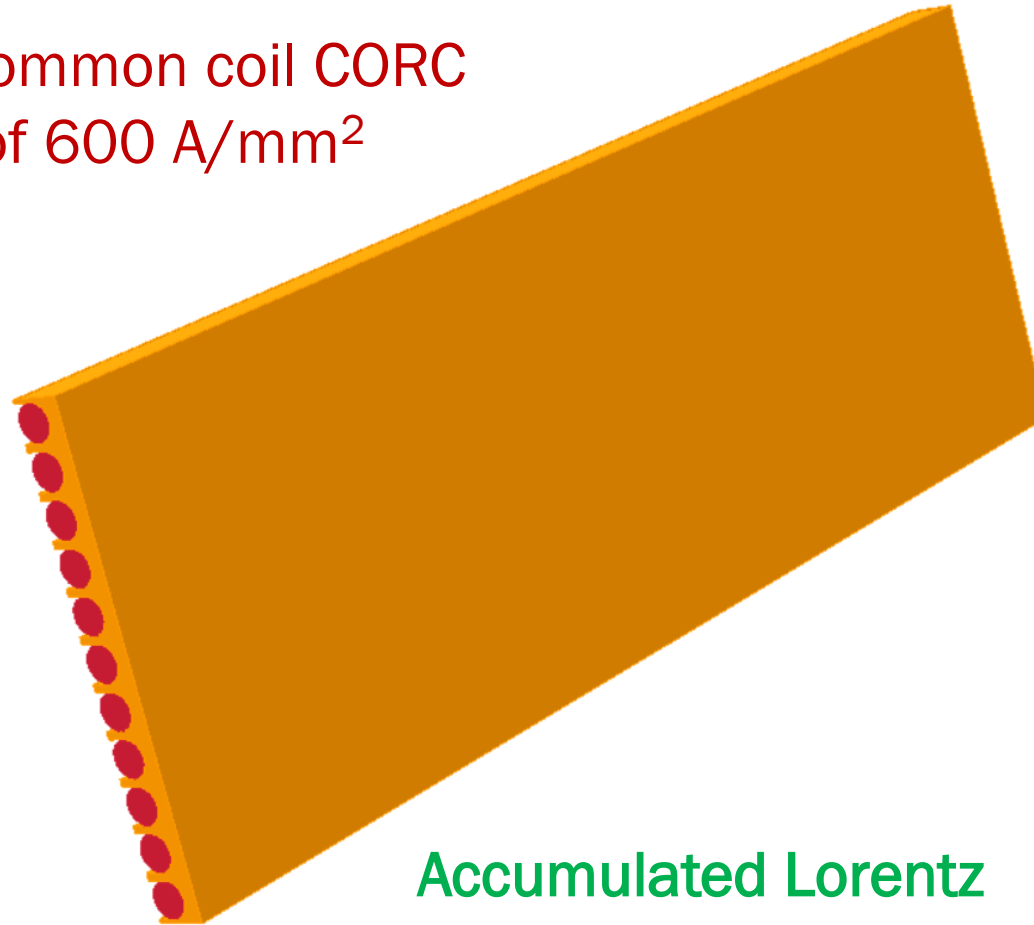
Overall Current density with structure:

- Area for 6 mm wire: $\pi \cdot 6^2 / 4 = 28.3 \text{ mm}^2$
- Area for 6.5mm X 8mm rectangle = 52 mm²

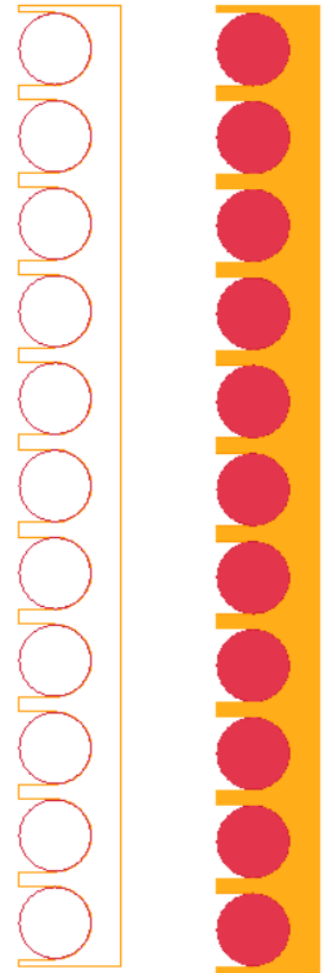
J_o for $J_e = 600 \text{ A/mm}^2$:

□ $J_o = 600 \cdot 28.3 / 52 = 326 \text{ A/mm}^2$

- Similar to Bi2212; but with a structure



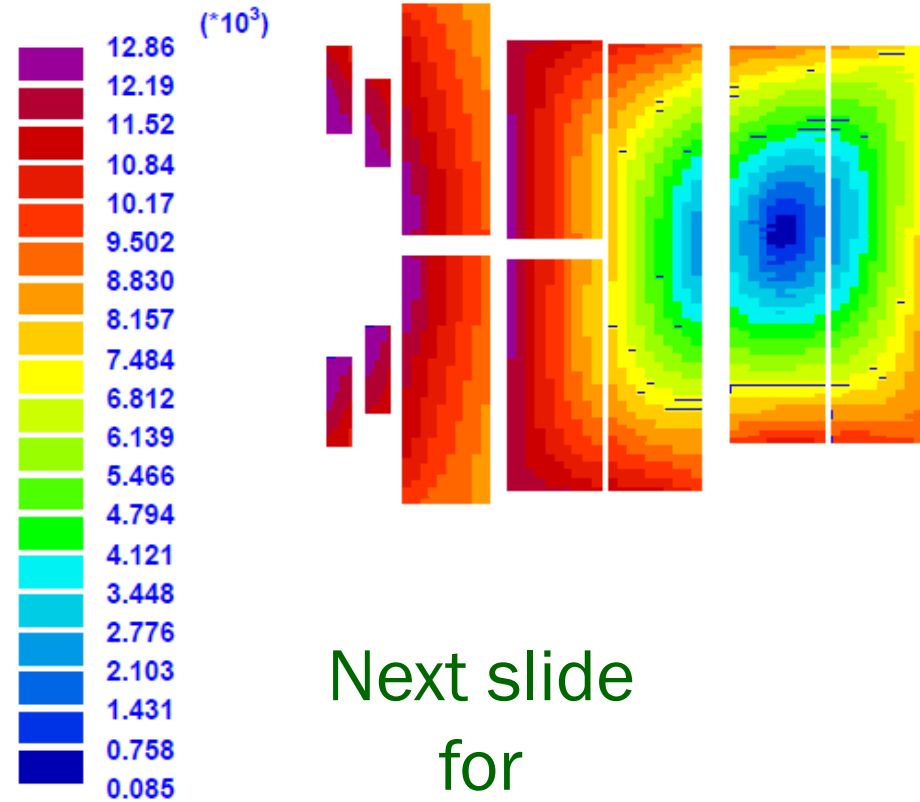
Accumulated Lorentz
forces can be managed
in a structure





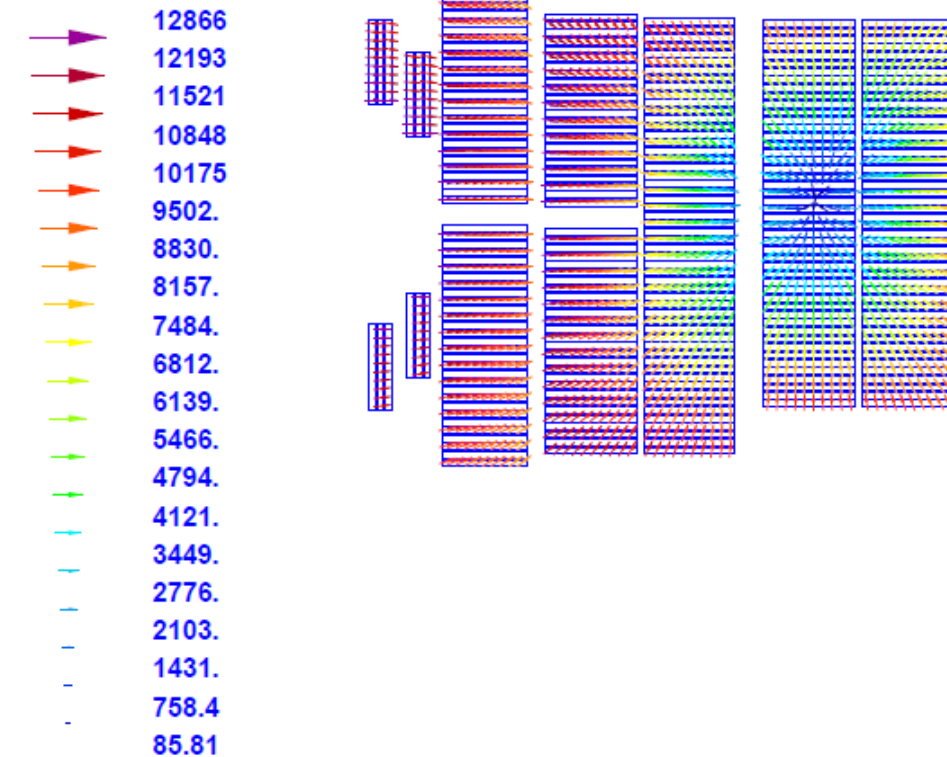
Lorentz Forces at the Design Field (2)

$|F| / L$ (N/M)



Next slide
for
 F_x and F_y

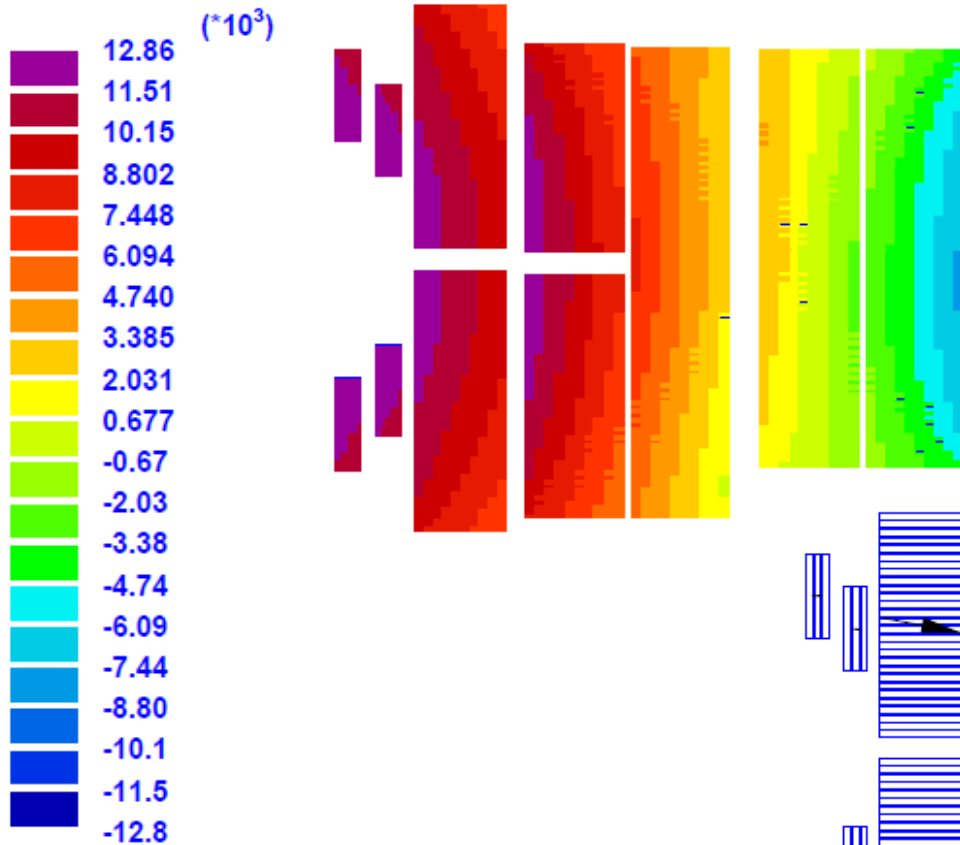
Emag. force / L (N/m)



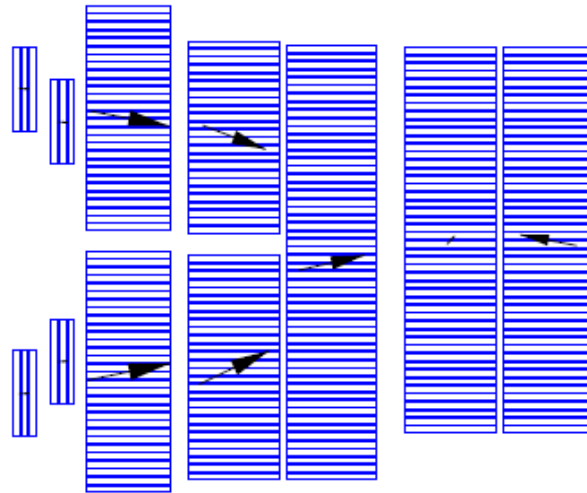
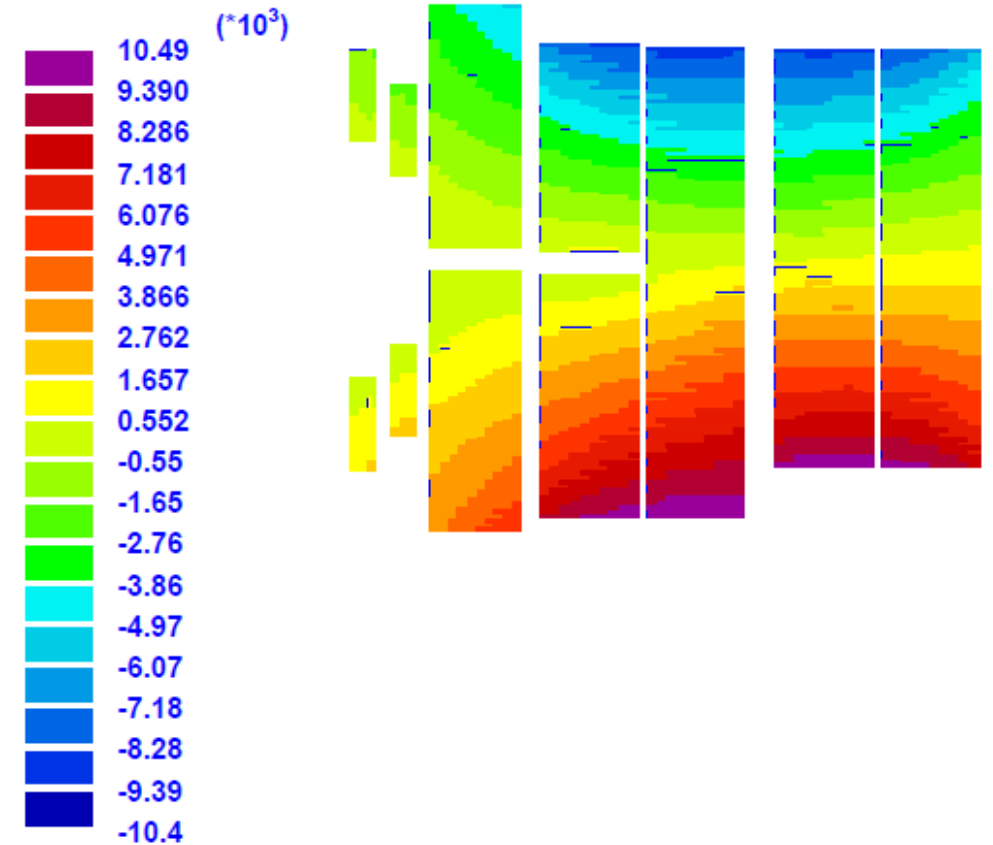


Lorentz Forces at the Design Field (1)

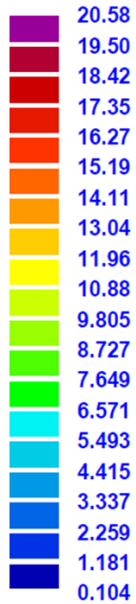
F_x / L (N/M)



F_y / L (N/M)



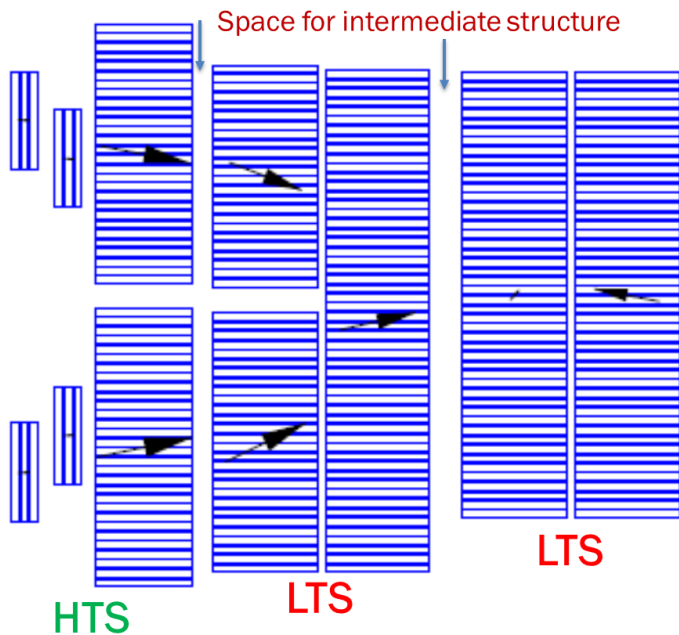
|B| (T)



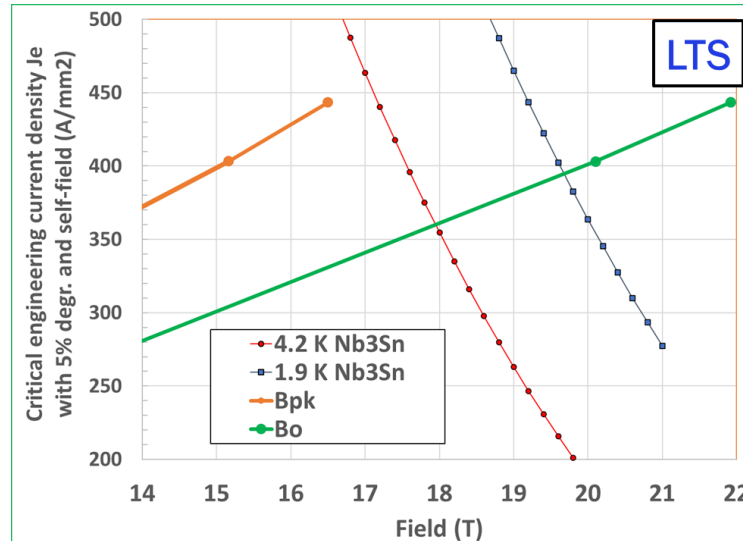
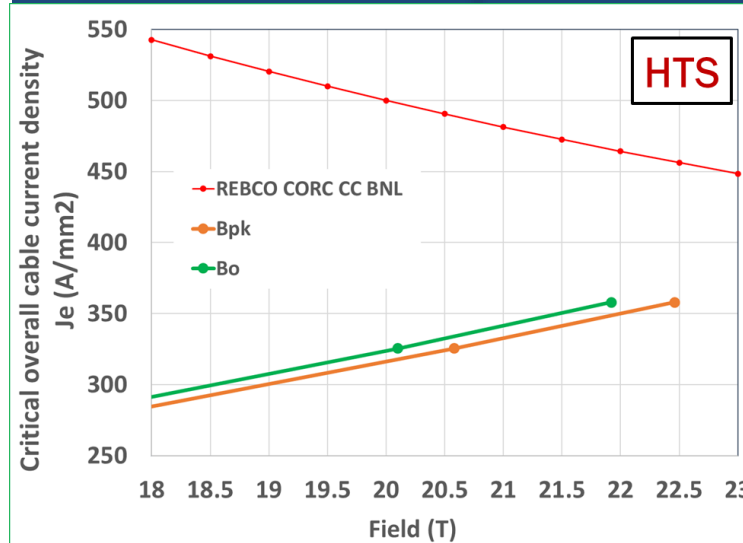
HTS

LTS

LTS

 $B_0 = 20.1\text{ T}$ $B_{pk} = 20.6\text{ T}$ $B_{pk} = 16.5\text{ T}$ $B_{pk} = 13.6\text{ T}$ 

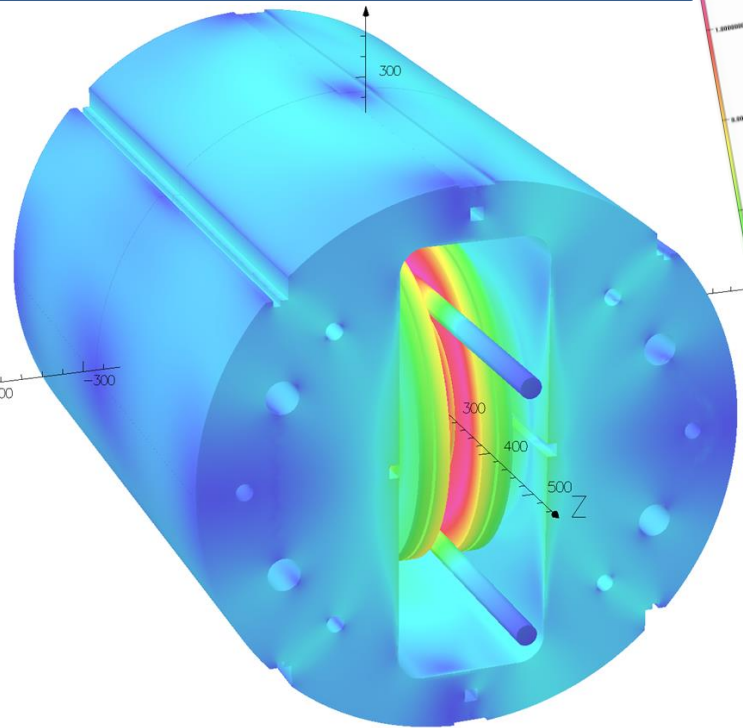
Key Benefits of the Common Coil Design for HTS/LTS High Field Hybrid Dipoles



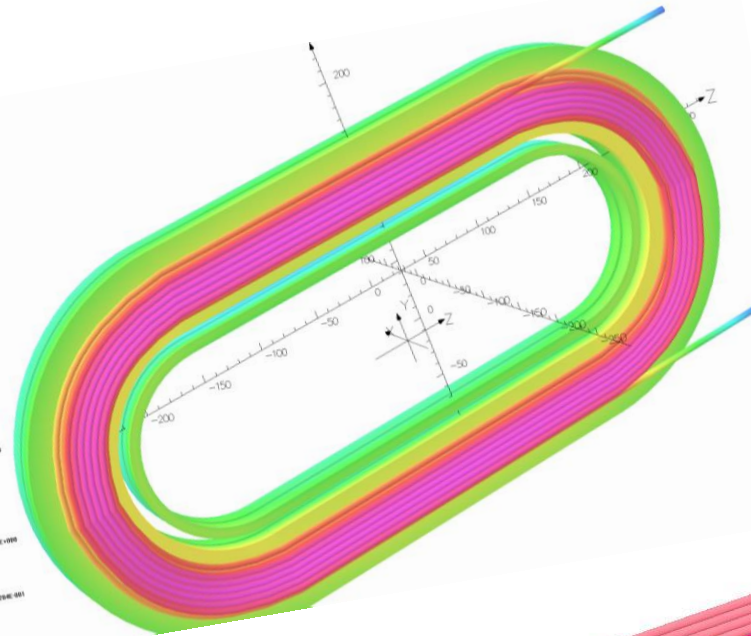
- Natural segmentation between HTS and LTS (and different cables)
- Easier tuning between HTS & LTS
- Coil layers move as a module without causing strain at ends (BNL common coil had 200 μm)
- Intermediate space for stress management structure. It can be easily adjusted, even at the late stage of the magnet construction

CORC Coil Programs with the Common Coil Dipole

STTR Coils two sets:
Each with 6 and 8 turns

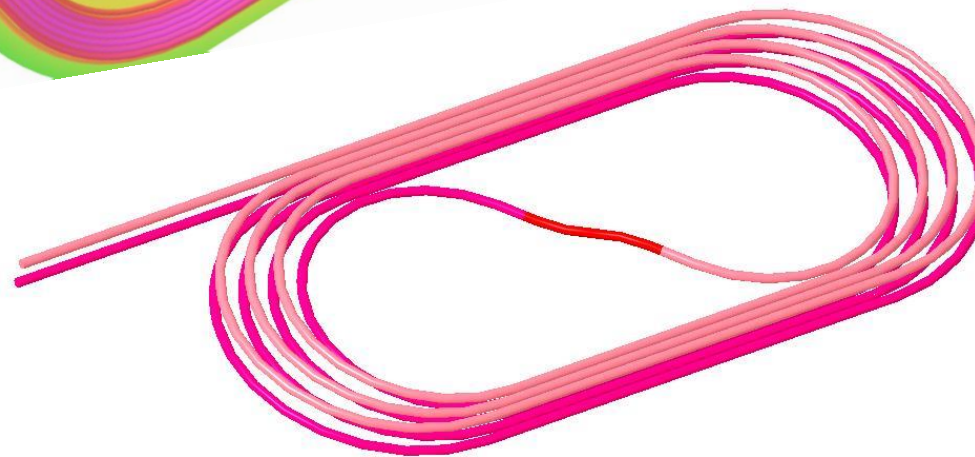


CORC[®] coils will run in series with the Nb₃Sn coils



**STTR: High field Demo
(13-14 T with 10 T from LTS)**

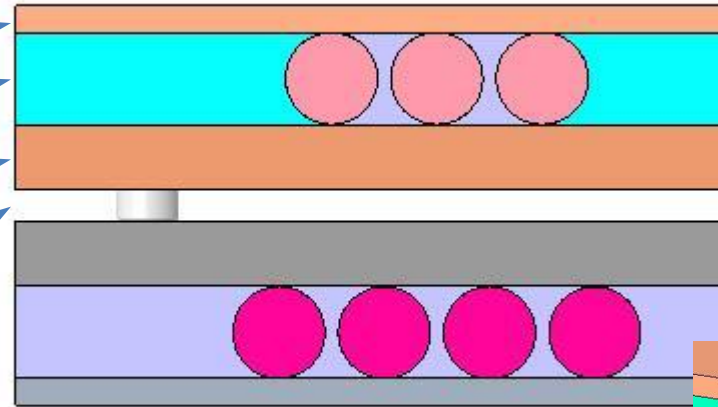
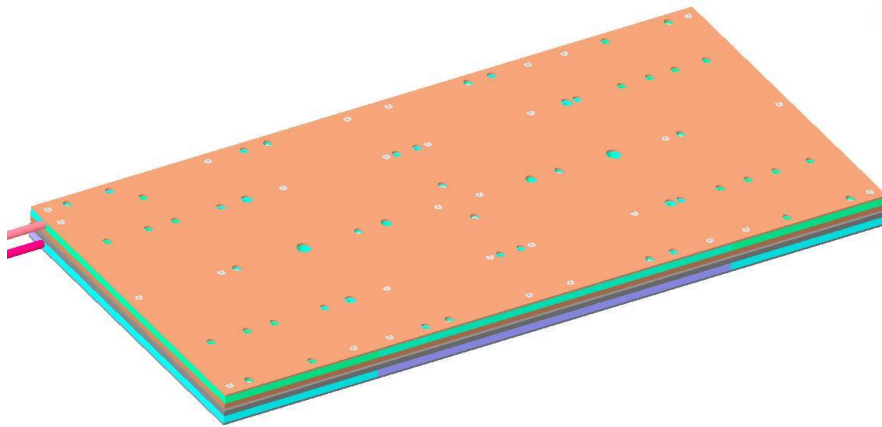
**MDP: Quench studies and
technology demo
(10.7 T with 10 T from LTS)**



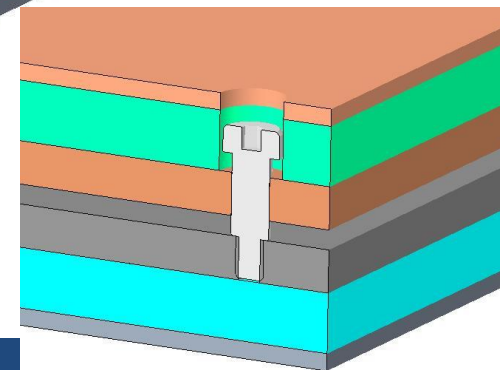
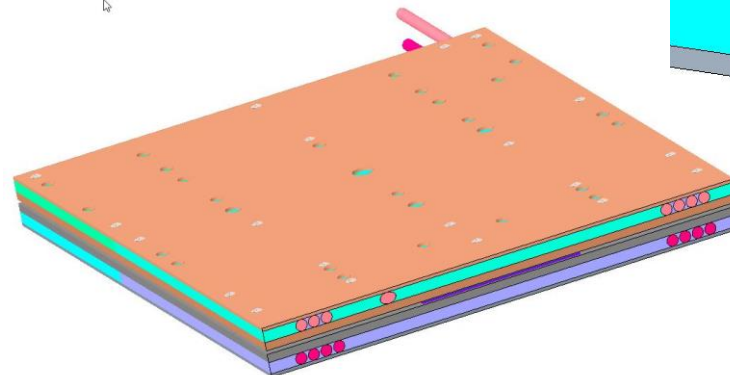
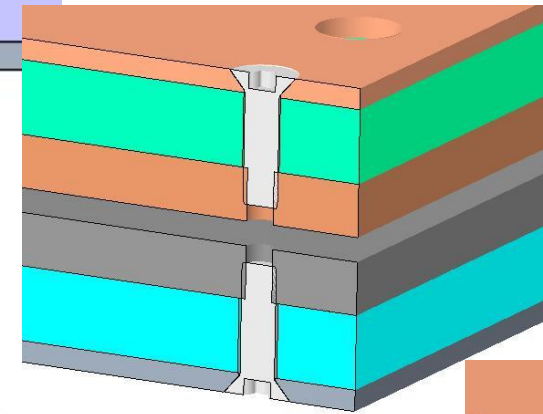
**MDP Coil
4+4 turns
with an S-turn**

CORC Coil Package (MDP)

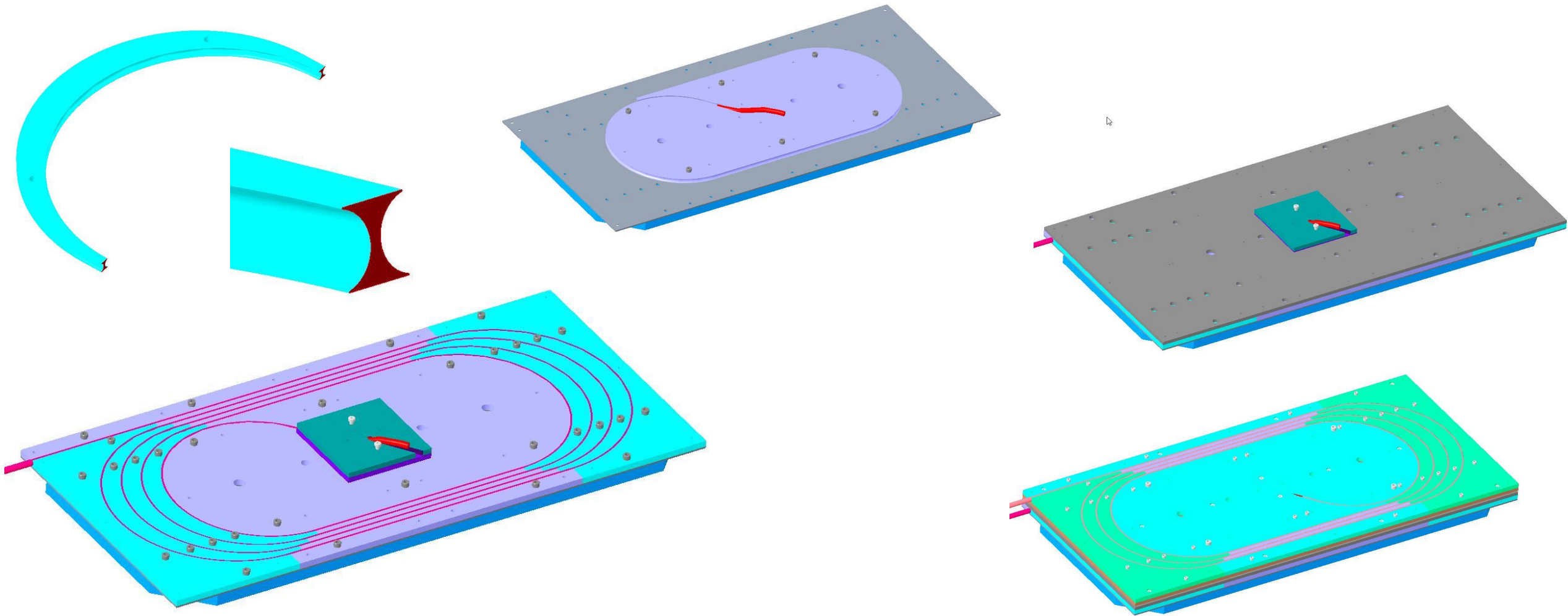
- Overall thickness – 30.3 mm
- Outer plates – 2 mm
- Coil spacers – 7 mm
- Inner plates – 5 mm
- Gap between layers – 2.3 mm



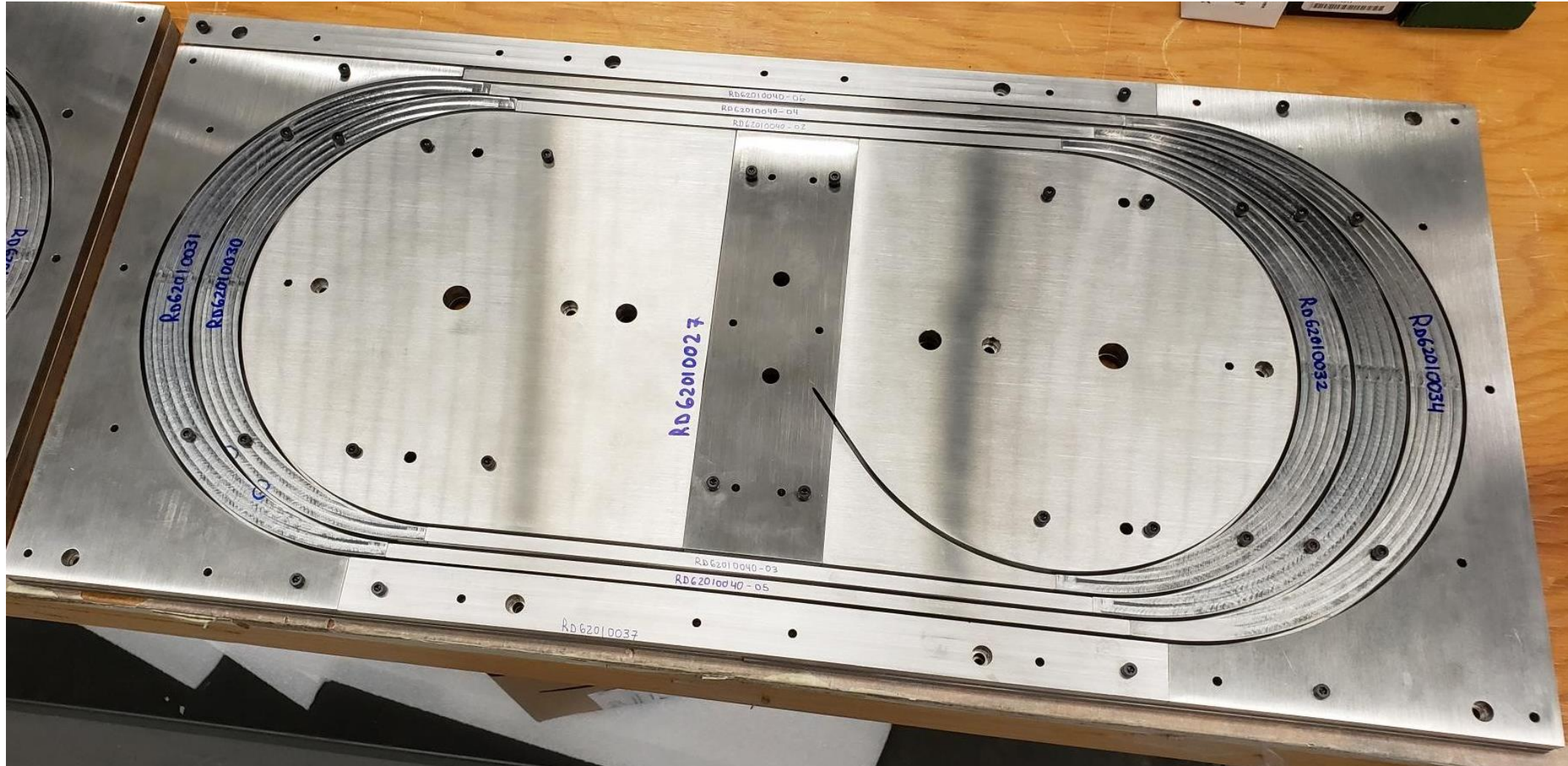
- Each layer held together with flat head screws
- Assembly held with shoulder screws to allow separation of layers.



Coil & Structure Parts, as Designed



Parts, as Made or Delivered (all parts in hand now)



Parts for one-side of the coil

Summary and Discussion

Observations on the HTS/LTS hybrid common coil design presented today:

- The design provides the desired margin for both HTS and Nb_3Sn , even at 4 K
- Same magnetic design is used for both CORC and Bi2212
 - Common coil design allows higher J_e or higher J_o for CORC
- The design is reasonably well optimized for a good field quality
- We, however, should be able to optimize the conductor usage as LTS coils still have room. As such the common coil design is well suited for hybrid designs.
- Space for the managed structure is included and more/less can be adjusted, as needed
 - Next Step – mechanical analysis and structure design
 - Expect that the magnetic and mechanical design to be iterated together
- Stress management should be relatively easier and effective in the common coil design
- All files (ROXIE, EXCEL, etc.) are available for sharing