

## **US LHC Accelerator Research Program**

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# A Review of Open Midplane Dipole Design Study

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## Overview

High luminosity Interaction Regions present a hostile environment for superconducting magnets due to large amount of particle spray from p-p collisions:

- "Dipole First Optics" reduces long-range beam-beam effects and makes correction of field errors in quadrupole more robust.
- Heat removal poses a significant challenge, both in terms of technical performance and in terms of economical operation of IR magnets.

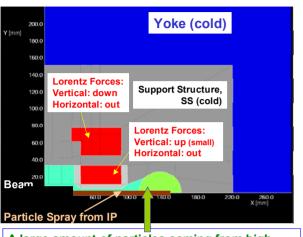
This presentation should provide a brief review of (a) the basic features of "Open Midplane Dipole Design" and (b) progress made in last few years.

The intend audience is beam physicists and intended purpose is to let them know the status/possibilities of such a design and to seek feedback.

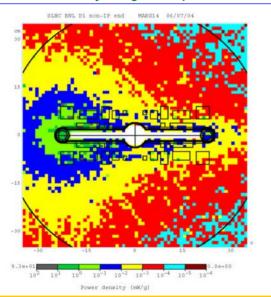
At this stage there is no plan to do build any such R&D magnet.



# Open Midplane Dipole for LHC Luminosity Upgrade Basic Design Features and Advantages



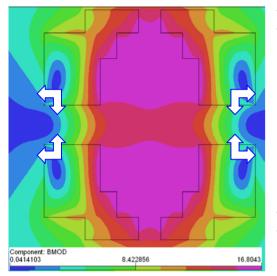
A large amount of particles coming from high luminosity IP deposit energy in a warm (or 80 K) absorber, that is inside the cryostat. Heat is removed efficiently at higher temperature.



- ☐ In the proposed design the particle spray from IP deposits most of its energy in a warm absorber, whereas in the conventional design most of the energy is deposited in coils and other cold structures.
- □ Calculations for the dipole first optics show that the proposed design can tolerate ~ 9kW/side energy deposited for 10<sup>35</sup> upgrade in LHC luminosity, whereas in conventional designs it would cause a large reduction in quench field.
- □ The requirements for increase in CERN cryogenic infrastructure and in annual operating cost would be minimum for the proposed design, whereas in conventional designs it will be enormous.
- The cost & efforts to develop an open midplane dipole must be examined in the context of overall accelerator system rather than just that of various magnet designs.

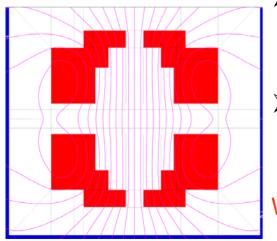


# Open Midplane Dipole Design Challenges



- Attractive vertical forces between upper and lower coils are large than in any high field magnet. Moreover, in conventional designs they react against each other. Containing these forces in a magnet with no structure between the upper and lower coils appears to be a big challenge.
- The large gap at midplane appears to make obtaining good field quality a challenging task.
- ➤ The ratio of peak field in the coil to the field at the center of dipole appears to become large as the midplane gap increases.
- Designs may require us to deal with magnets with large aperture, large stored energy, large forces and large inductance.

With these challenges in place, don't expect the optimum design to necessarily look like what we are used to seeing.





# LARP Dipole Design Development

The design is being developed in a comprehensive and iterative way, where

- energy removal
- magnetic
- mechanical
- and beam physics

requirements are optimized together.

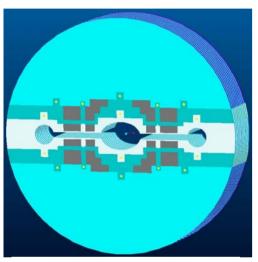
There are no rules, past experience or guidelines to follow.

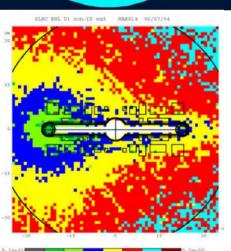
Given that it's a new type of design, old approaches may not always provide the best or even a working solution.



# A True Open Midplane Design

# By open midplane, we mean truly open midplane:





Particle spray from IP (mostly at midplane), pass through an open region to an absorber sufficiently away from the coil without hitting anything at or near superconducting coils.

In earlier "open midplane designs", although there was "no conductor" at the midplane, but there was some 'other structure" between the upper and lower halves of the coil. Secondary showers from that other structure deposited a large amount of energy on the coils.

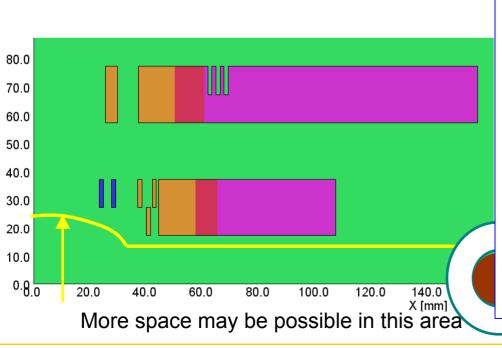
The energy deposited on the superconducting coils by this secondary shower became a serious problem. Therefore, the earlier open midplane designs were not that attractive.



# Magnetic Design and Field Quality

A critical constraint in developing magnetic design of an open midplane dipole with good field quality is the size of the midplane gap for coil.

The desired goal is that the gap is large enough so that most showers pass through without hitting anything before hitting the warm target.



Coil-to-coil gap in latest design = 34 mm (17 mm half gap)

**Horizontal aperture = 80 mm** 

•Vertical gap is > 42% of horizontal aperture (midplane angle: 23°)

This makes obtaining a high field and a high field quality a kind challenging task!

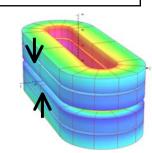
What part of cosine  $(\theta)$  is left in that cosine  $(\theta)$  current distribution now?



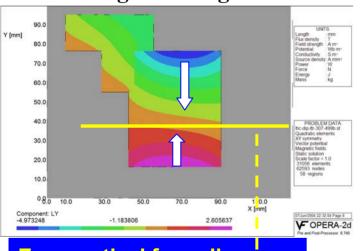
# Navigation of Lorentz Forces

### A new and major consideration in design optimization

Unlike in conventional designs, in a truly open midplane design the upper and lower coils do not react against each other. As such this would require a large structure and further increase the coil gap. That makes a good field quality solution even more difficult.

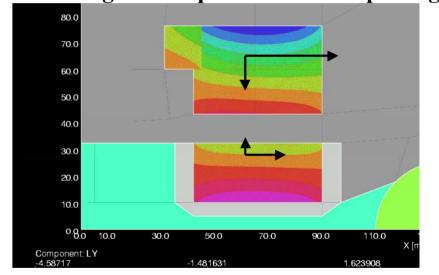






# Lorentz force density (Vertical)

#### New Design Concept to reduce midplane gap



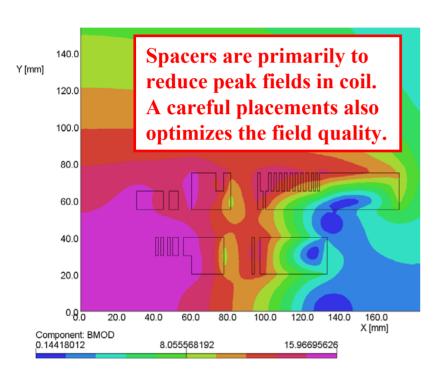
#### Zero vertical force line

Since there is no downward force on the lower block (there is slight upward force), we do not need much support below it, if the structure is segmented. The support structure can be designed to deal with the downward force on the upper block using the space between the upper and the lower blocks.

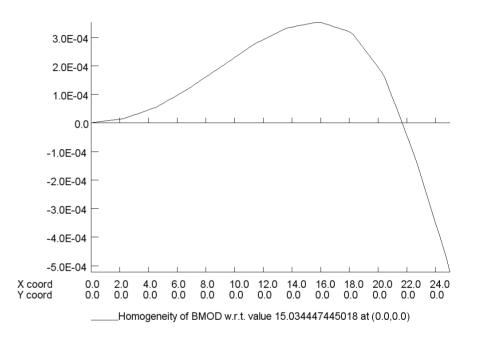


# Peak Field Enhancement and Field Quality

#### Field Contour at 15 T Central Field



#### Field Errors at the Midplane



**Peak Field Enhancement:**  $16T/15T = \sim 6.6\%$ 

(a typical value is obtained despite a large midplane gap) Appears to meet the present design guidance. Detailed field harmonics are yet to be optimized. However, 10<sup>-4</sup> relative errors at midplane suggest that we should be able to meet the typical goals.



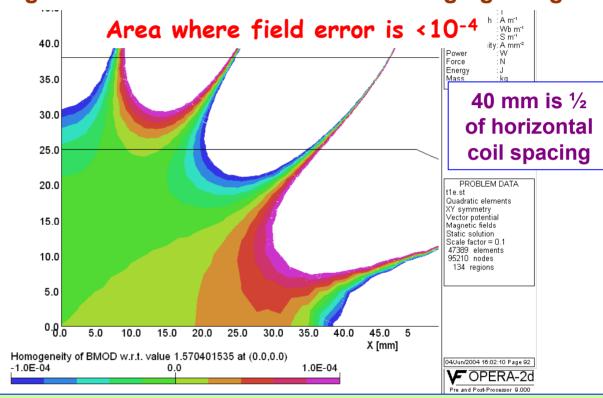
# Field Harmonics and Relative Field Errors In An Optimized Design

#### Proof: Good field quality design can be obtained in such a challenging design:

(Beam @ x=+/- 36 mm at far end) (Max. radial beam size: 23 mm)

#### **Geometric Field Harmonics:**

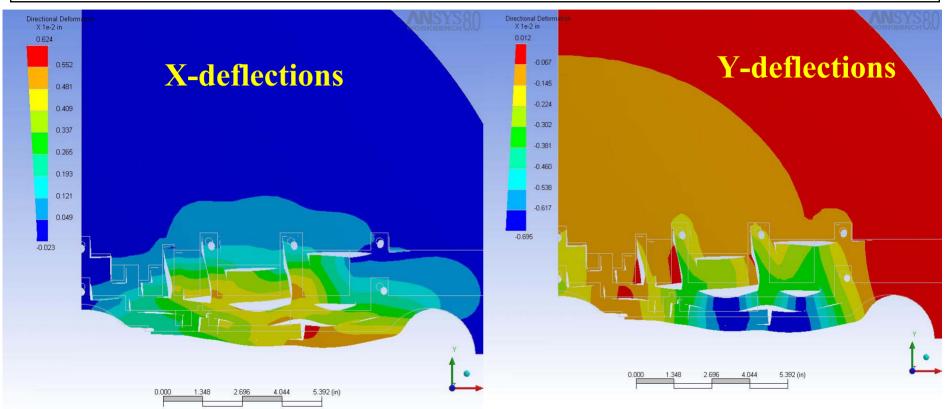
	Ref(mm)	Ref(mm)					
n	36	23					
1	10000	10000					
2	0.00						
3	0.62	0.25					
4	0.00	0.00					
5	0.47	80.0					
6	0.00	0.00					
7	0.31	0.02					
8	0.00	0.00					
9	-2.11	-0.06					
10	0.00	0.00					
11	0.39	0.00					
12	0.00	0.00					
13	0.06	0.00					
14	0.00	0.00					
15	-0.05	0.00					
16	0.00	0.00					
17	0.01	0.00					
18	0.00	0.00					
19	0.00	0.00					
20	0.00	0.00					



Field errors should be minimized for actual beam trajectory & beam size. It was sort of done when the design concept was being optimized by hand. Optimization programs are being modified to include various scenarios. Waiting for feed back from Beam Physicists on how best to optimize. However, the design as such looks good and should be adequate.



# Mechanical Analysis



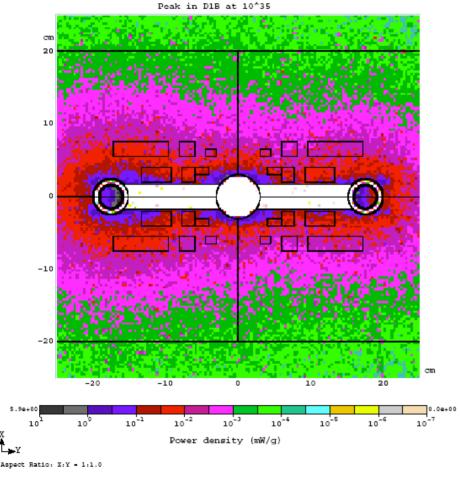
In the present design the relative values of the x and y deflections are 3-4 mil (100 micron) and the maximum value is 6-7 mil (170 micron).

Above deflections are at design field (13.6 T). They are  $\sim$ 1-2 mil higher at quench field.

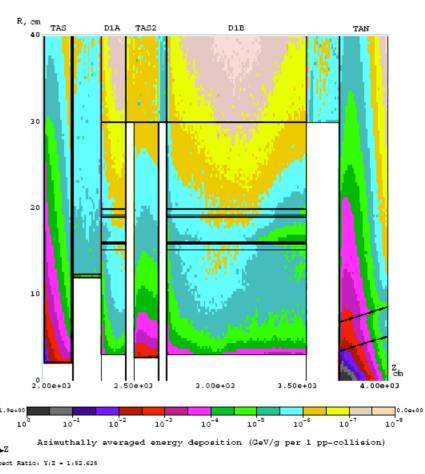


# Energy Deposition in Open Midplane Dipole in Dipole First Optics

#### Courtesy: Nikolai Mokhov, FNAL



Power density isocontours at the non-IP end of the D1B.



Azimuthally averaged energy deposition iso-contours in the dipole-first IR.



# Energy Deposition Summary (Mokhov, 04/05)

#### SUMMARY

- The open midplane dipole is very attractive option for the LARP dipole-first IR at  $\mathcal{L} = 10^{35}$ . The design accommodates large vertical forces, has desired field quality of  $10^{-4}$  along the beam path and is technology independent.
- After several iterations with the BNL group over last two years, we have arrived at the design that – being more compact than original designs – satisfies magnetic field, mechanical and energy deposition constraints.
- We propose to split the dipole in two pieces, 1.5-m D1A and 8.5-m D1B, with a 1.5-m long TAS2 absorber in between.
- With such a design, peak power density in SC coils is below the quench limit with a safety margin, heat load to D1 is drastically reduced, and other radiation issues are mitigated. This is a natural two-stage way for the dipole design and manufacturing.





# Summary of Design Iterations (A to F)

	A	В	C	D	E	F
H(mm)	84	135	160	120	80	120
V(mm)	33	20	50	30	34	40
V/H	0.39	0.15	0.31	0.25	0.43	0.33
$B_{o}(T)$	13.6	13.6	13.6	13.6	15	13.6
$B_{ss}(T)$	15	15	15	14.5	16	15
$J_{c}(A/mm^{2})$	2500	3000	3000	3000	3000	3000
Cu/Sc	1	1,1.8	0.85	0.85	0.85	1
A(cm <sup>2</sup> )	161	198	215	148	151	125
$R_i(mm)$	135	400	400	320	300	300
R <sub>o</sub> (mm)	470	800	1000	700	700	700
E(MJ/m)	2.2	4.8	9.2	5.2	4.1	4.8
$F_x(MN/m)$	9.6	10.1	12.3	9.5	10.4	9.6
$F_{y}(MN/m)$	-3.0	-6.8	-8.7	-7.0	-5.1	-5.4



## Lower Field (lower cost) Open Midplane Dipole?

Is it worthwhile to examine lower field open midplane dipole?

➤ Lower field/lower aperture magnet will be cheaper.

~ 8 T open midplane dipole can possibly be built with NbTi Technology.



#### SUMMARY of the Presentation

The "Open Midplane Dipole Design" offers a good technical and an economical option for LHC luminosity upgrade in "Dipole First Optics"

- The challenging requirements of the design have been met:
  - > A design that can accommodate a large gap between upper and lower coils with no structure in between.
  - > A design with good field quality design despite a large midplane gap.
  - > Energy deposition on the s.c. coils can be kept below quench limit and the component lifetime can be kept over 10 years.
  - Heat can be economically removed at a higher temperature with a warm absorber within coldmass.
- A proof of principle design has been developed and many iterations have been carried out to optimize the overall parameter space.
- The design brings a significant new addition to magnet technology.