

# HTS in a Variety of Future Accelerator Magnets

Ramesh Gupta

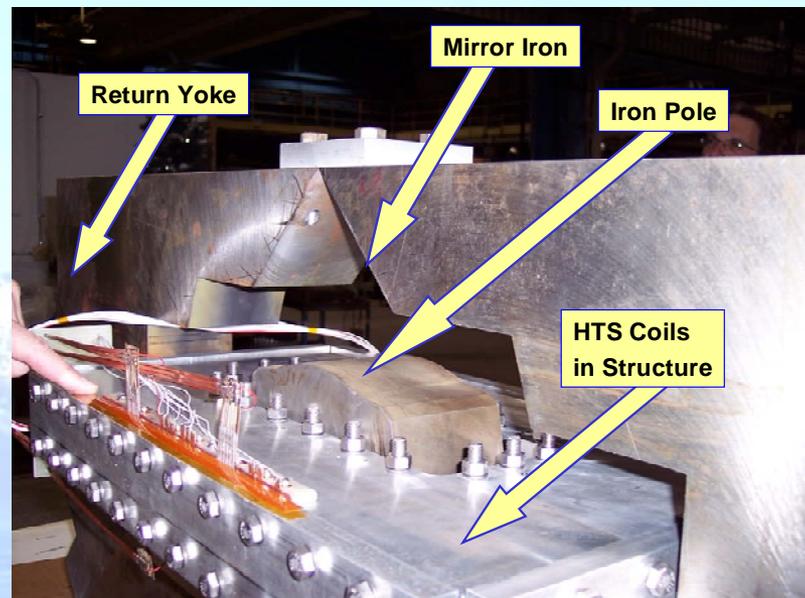
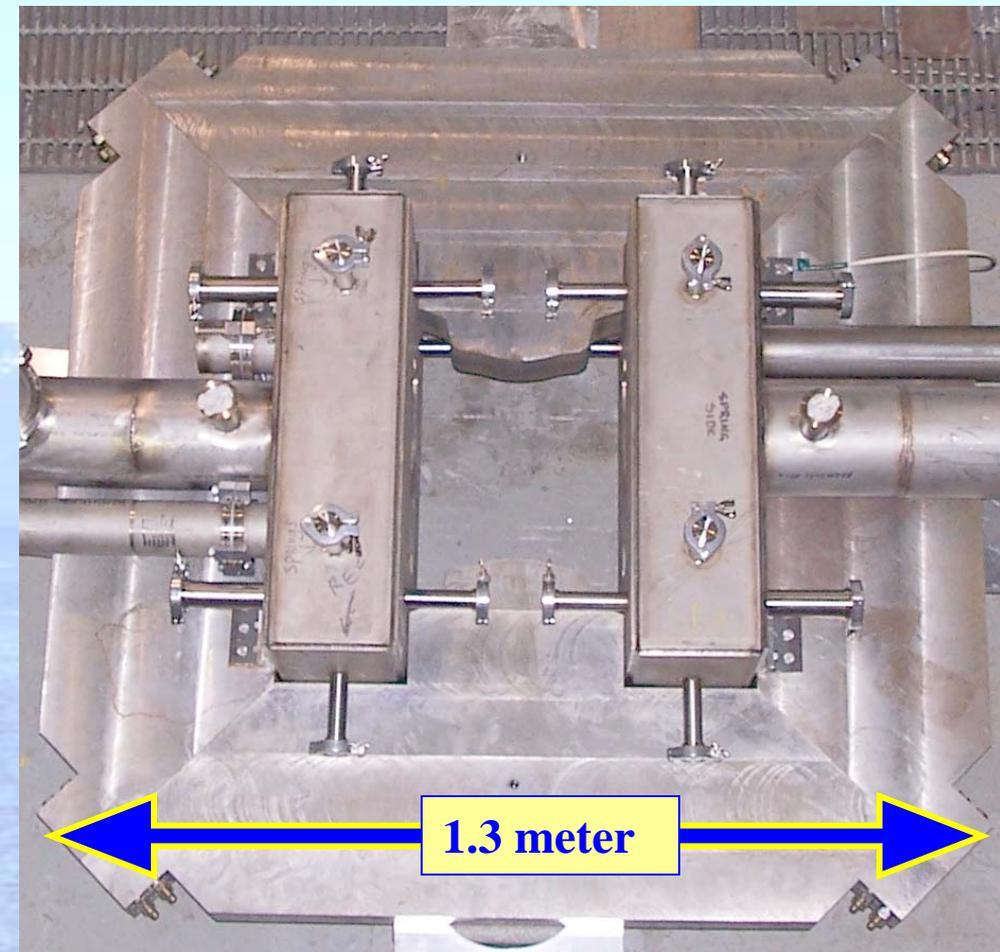
LTSW 2007 @ Lake Tahoe

# HTS in a Variety of Magnets

- **HTS in very high field magnets**
    - no superconductor can carry such high current density at very high fields.
  - **HTS in magnets subjected to high heat loads**
    - no superconductor can tolerate such high heat loads + local temperature rise and then remove energy so efficiently.
  - **HTS in energy efficient magnets**
    - low field (1-2 T) water-cooled cooper magnets for beam-lines and accelerator are becoming prohibitive to operate.
- ...and a combination of above.**

- **Experience with HTS R&D Magnets**
  - **RIA/FRIB Magnets (HTS for large heat loads)**
    - made with Bi2223 tape and now with YBCO Tape
  - **Common Coil Dipole (HTS for high field)**
    - made with Bi2212 Rutherford Cable
- **Future Possibilities for Accelerator Magnets**
  - **High Field Magnets**
    - with Bi2212 cable or YBCO *wide tape/* or *Roebel cable*
  - **Energy Efficient Magnets**
    - with YBCO Tape

# RIA HTS Model Quadrupoles



Cold iron mirror model



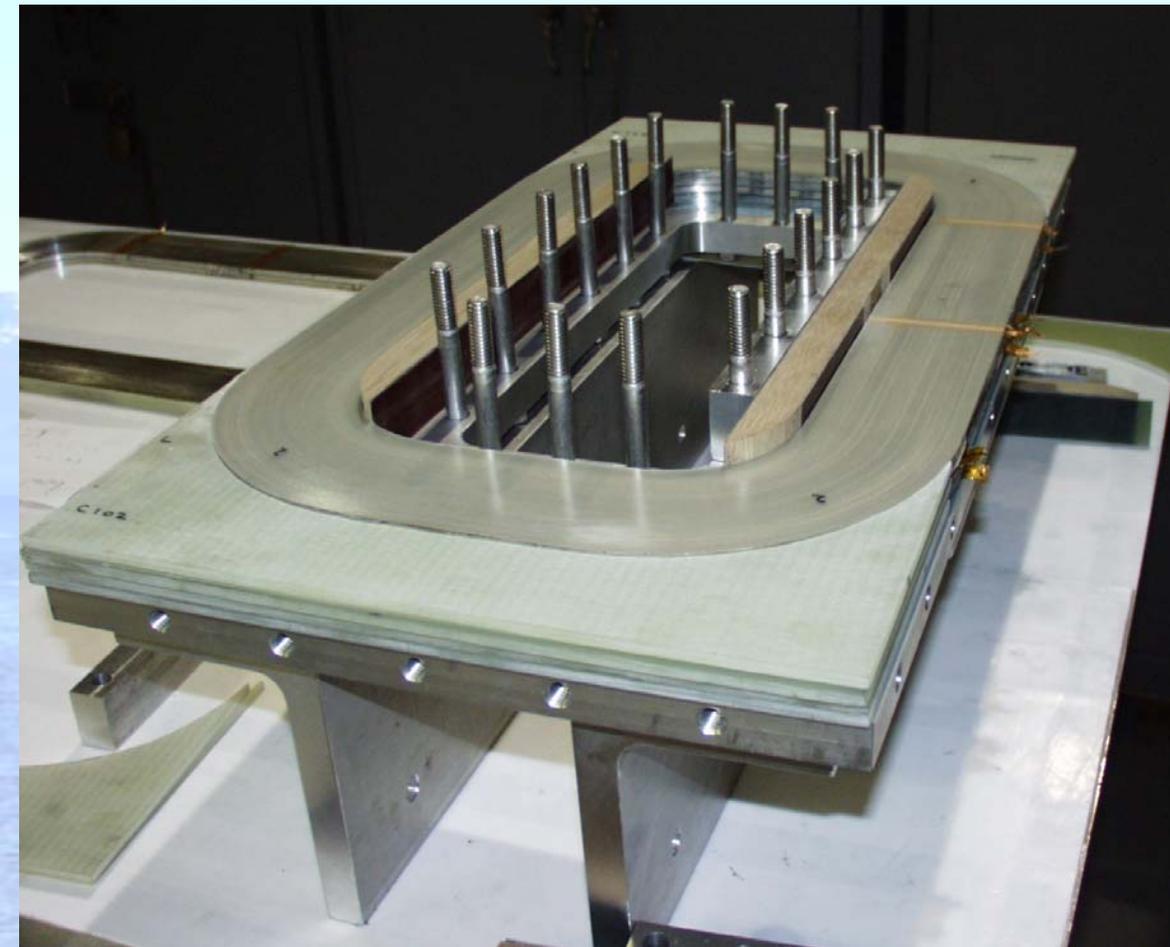
Warm iron mirror

**Warm iron R&D quadrupole with twenty four coils in two cryostats**

# Bi2223 Coils in RIA Quads

RIA quad is made with 24 coils with each using ~200 meter of commercially available HTS wire (tape).

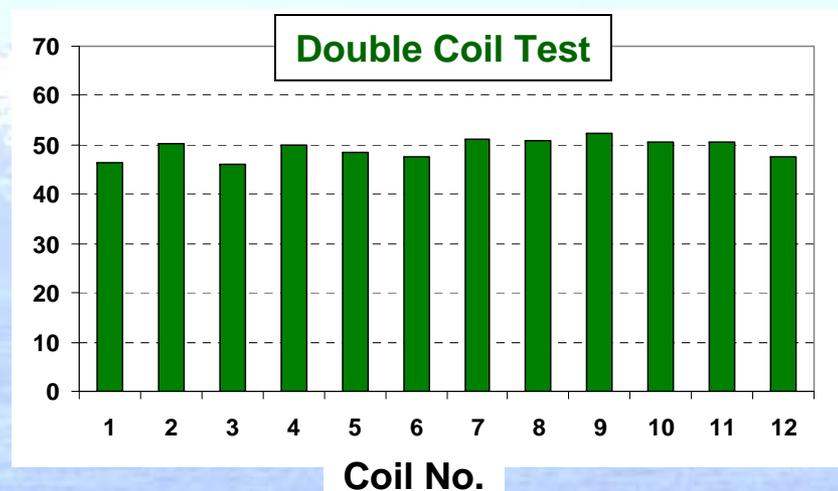
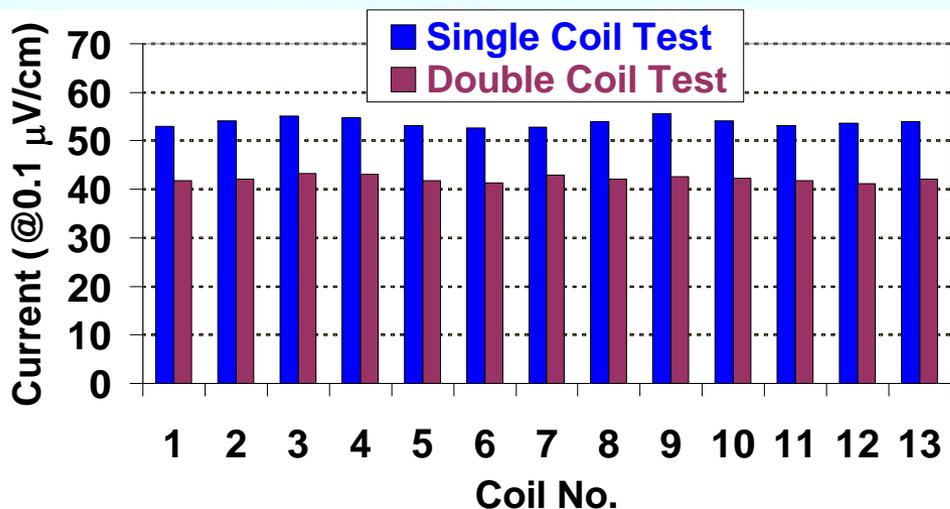
This gives a good opportunity to examine the reproducibility and reliability in performance of number of coils (number grows every year).



# LN<sub>2</sub> (77 K) Test of 25 BSCCO 2223 Coils

13 Coils made earlier tape  
(Nominal 175 turns with 220 meters)

12 Coils made with newer tape  
(150 turns with 180 meters)

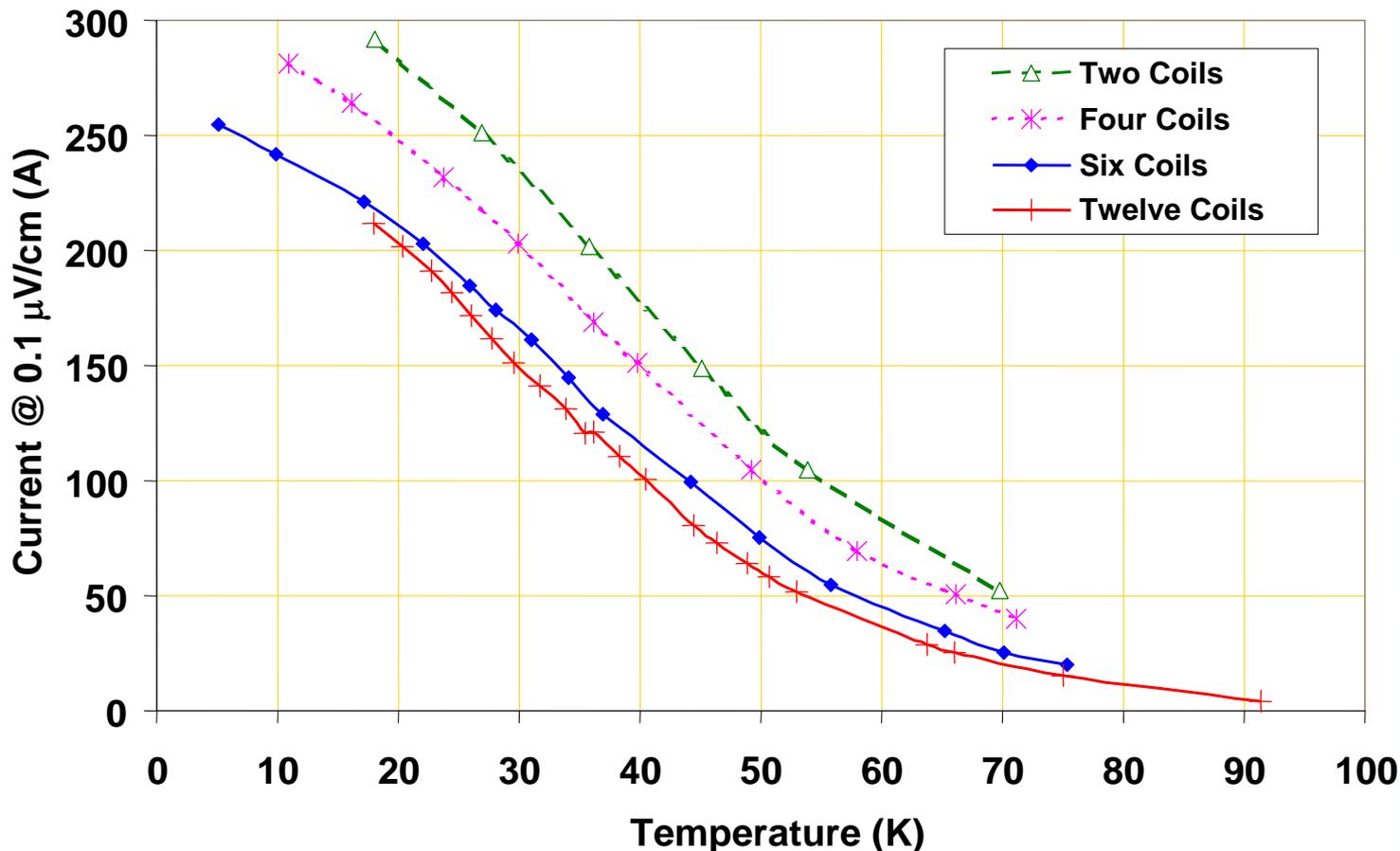


Coil performance generally tracked the conductor performance very well.

Note: A uniformity in performance of a large number of HTS coils made with commercially available superconductor (ASC).

It shows that the HTS technology is now maturing !

# RIA HTS Mirror Model Test Results (operation over a large temperature range)



More coils create more field and hence would have lower current carrying capacity

*A summary of the temperature dependence of the current in two, four, six and twelve coils in the magnetic mirror model. In each case voltage first appears on the coil that is closest to the pole tip. Magnetic field is approximately three times as great for six coils as it is for two coils.*

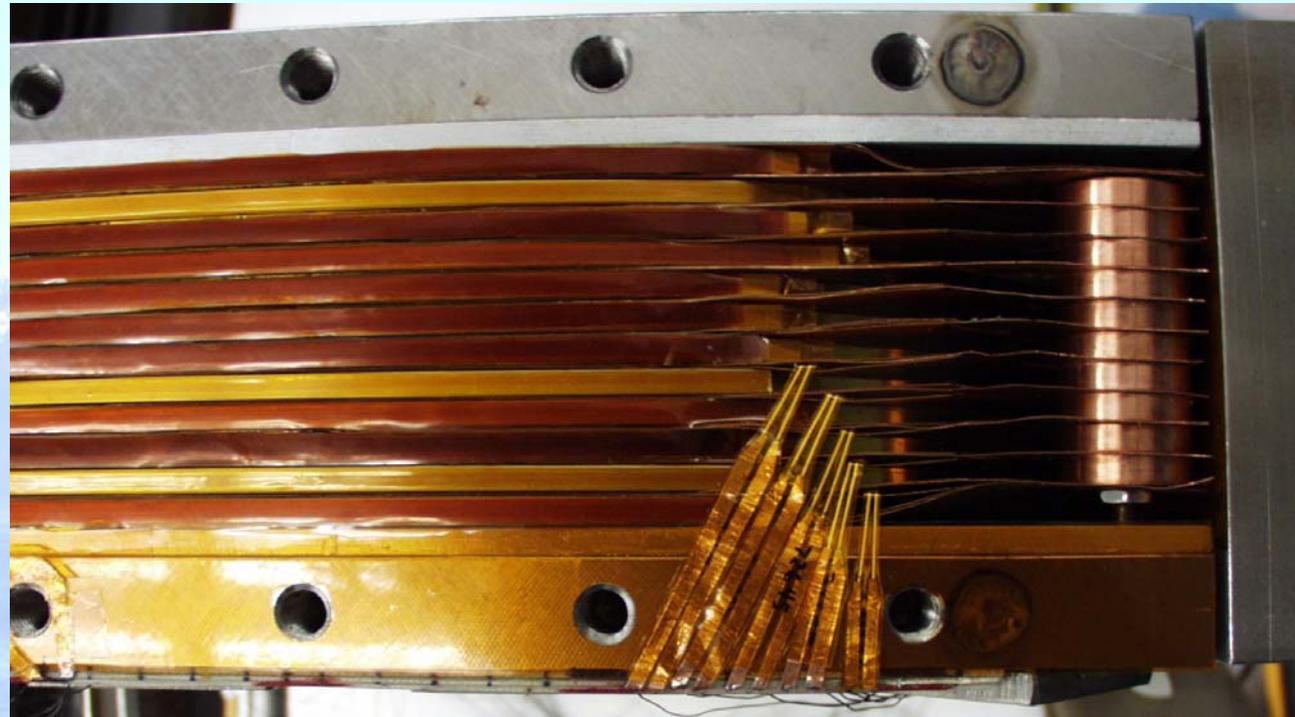
# Advantages of using HTS in RIA/FRIB

- Up to 400 kW of beam power hits the target producing a variety of isotopes. ~15 kW of the above is deposited in the first quadrupole itself.
- Removing these large heat loads at ~30 K (as in high temperature superconductors) instead of ~4K (as in low temperature superconductors) is over an order of magnitude more efficient.
- HTS can tolerate a large local increase in temperature in superconducting coils caused by the non-uniform energy deposition.
- Moreover, in HTS magnets, the temperature need not be controlled precisely. It can be relaxed by over an order of magnitude as compared to that for the present low temperature superconducting magnets (few kelvin rather than a few tenth of a kelvin). This simplifies the design and reduces cost of the cryogenic system.
- Therefore, HTS would facilitate a magnet system for fragment separator that will be robust and economical to operate.

## Energy Deposition and Cryogenic Experiments



**Stainless steel tape  
heaters for energy  
deposition experiments**



**Copper sheets between HTS coils with copper rods  
and copper washers for conduction cooling**

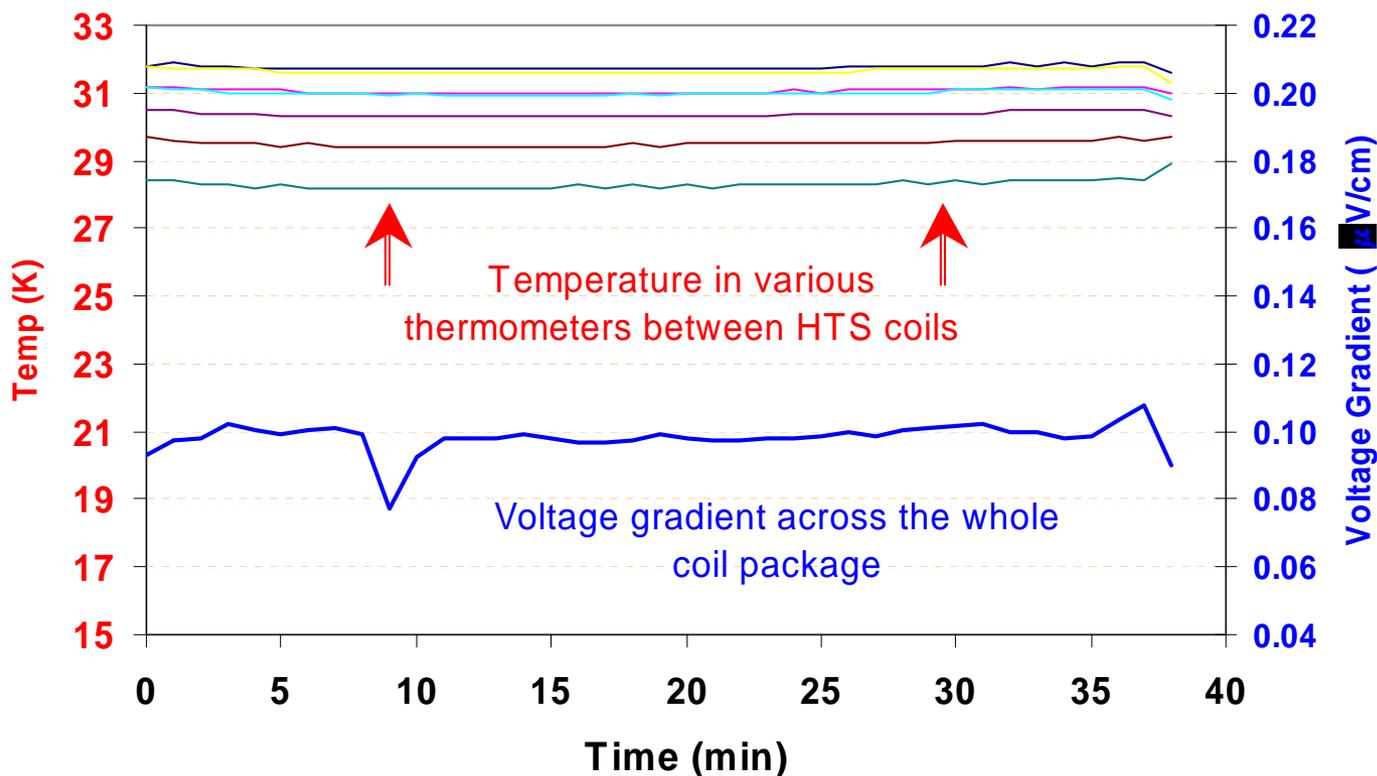
- **In conduction cooling mode, helium flows through top and bottom plates only.**
- **In direct cooling mode, helium goes in all places between the top and bottom plates and comes in direct contact with coils.**

# Large Energy Deposition Experiment

**Goal was to demonstrate that the magnet can operate in a stable fashion at the expected heat loads (5mW/cm<sup>3</sup> or 5kW/m<sup>3</sup> or 25 W on 12 short HTS coils) at the design temperature (~30 K) with some margin on current (@140 A, design current is 125 A).**

**Stable operation  
for ~40 minutes**

- We use 0.1  $\mu\text{V}/\text{cm}$  as the definition of  $I_c$
- Temperature differences may be partly real and partly calibration mis-match.
- As such HTS can tolerate such temp variations with small margin.



Voltage spikes are related to the noise

# FRIB/RIA with YBCO (2G)

**The goal is to move to 2<sup>nd</sup> generation (2G) wire because:**

- **2G is expected to allow operation at 50 K (or above), which would provide even more saving in operation.**
- **2G is expected to be less expensive.**

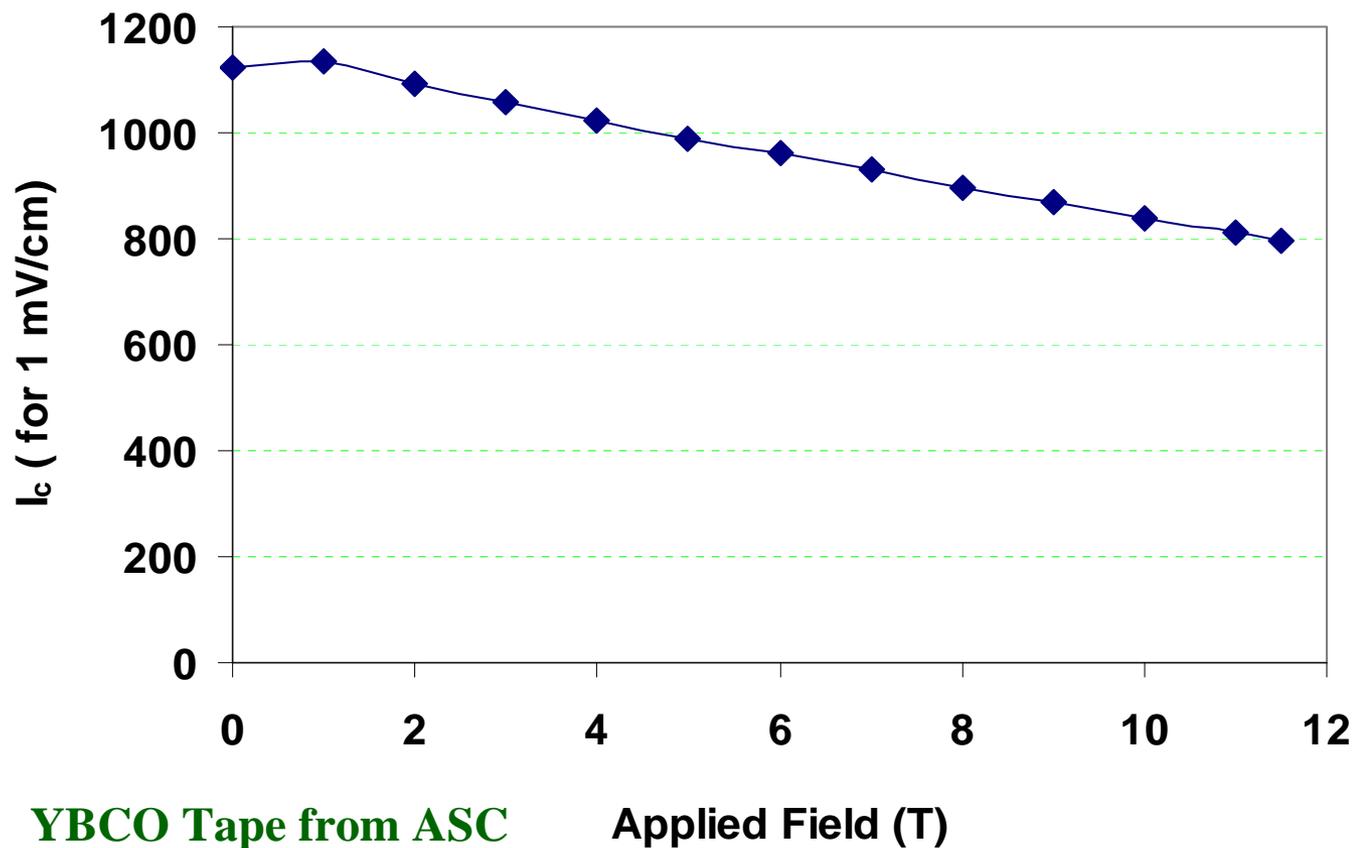
## Current YBCO Program

- **3 coils each with ~100 m of 2<sup>nd</sup> generation wire (initial plan was to make two coils only but the price conductor dropped that allowed us to re-scope the program).**
- **2 coils with wire from ASC and 1 from SuperPower.**
- **1 coil made with ASC wire (tape) has been built and tested (over a large range of temperature).**



**Coil made with 2G wire**

# YBCO Tape at 4K : $I_c$ Vs. $B_{\text{parallel}}$

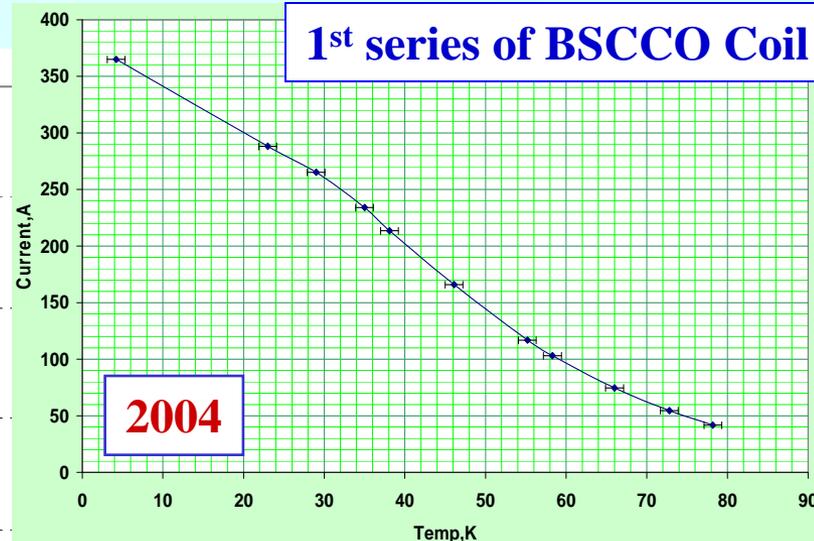
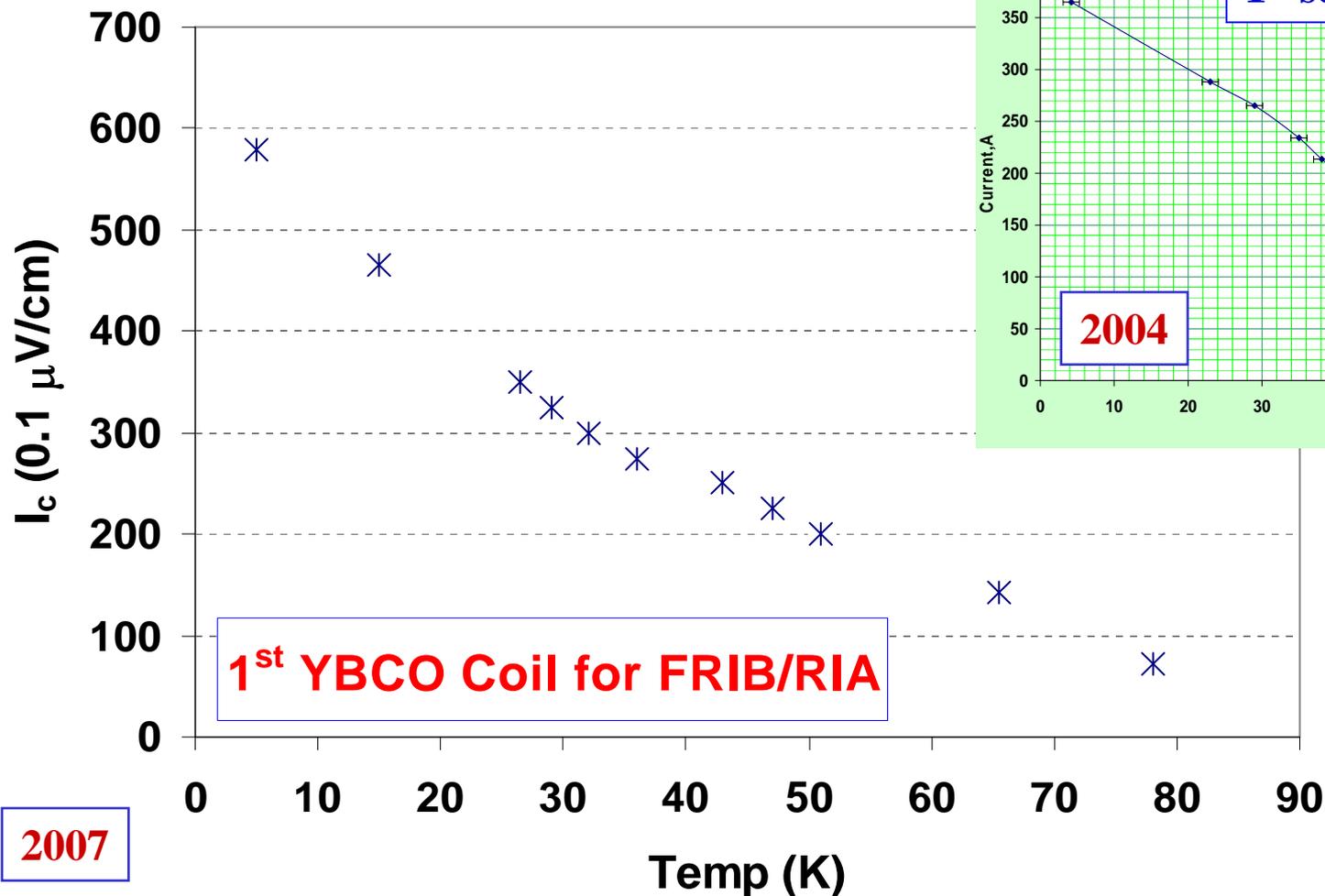


Small field dependence in field parallel direction.

Somewhat worse dependence in field perpendicular direction, however, nothing compared to that in LTS.

Measurements courtesy Ghosh and Sampson

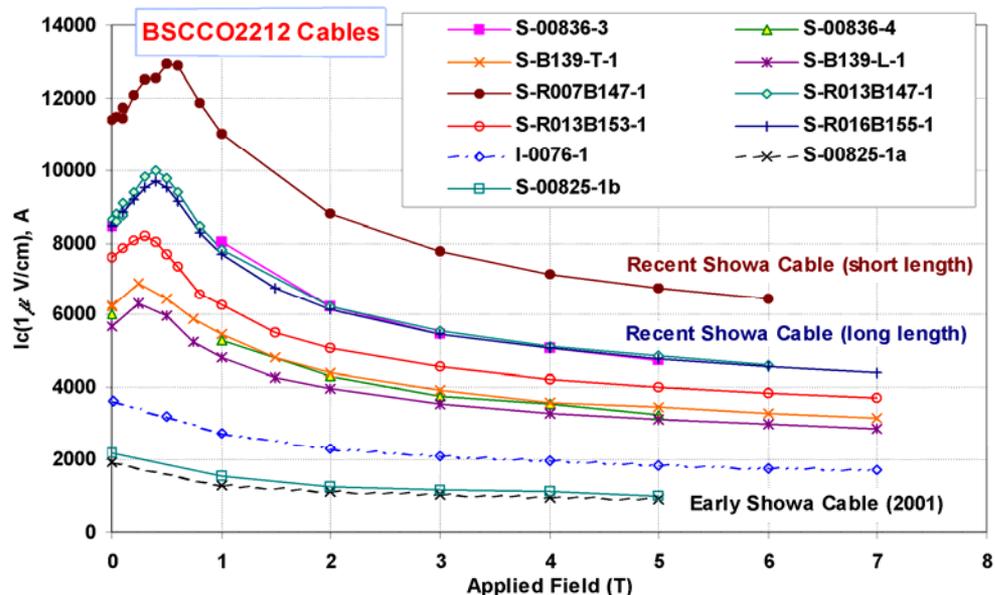
# $I_c$ Vs. T Over a Large Range of Temperature in RIA Coils Made with YBCO and Bi2223



**Note: YBCO is already better than BSCCO.**  
**And there is still a significant potential for improvements.**

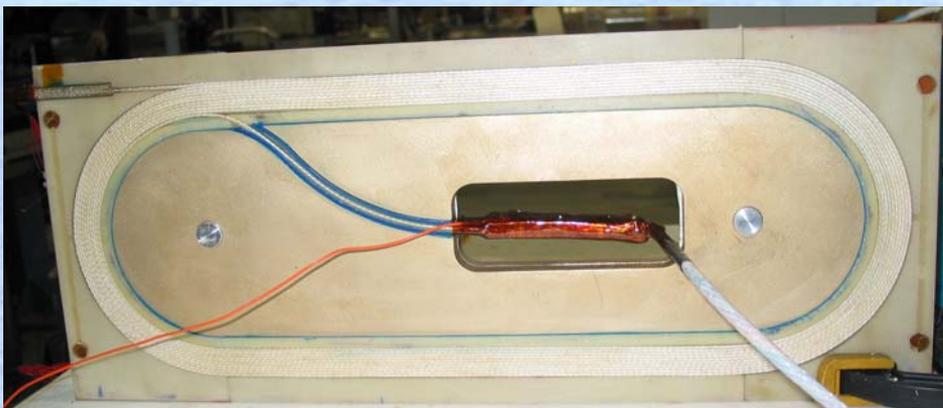
**BSSCO and YBCO Tapes from ASC**

# HTS for High Field Magnets with Rutherford Cable

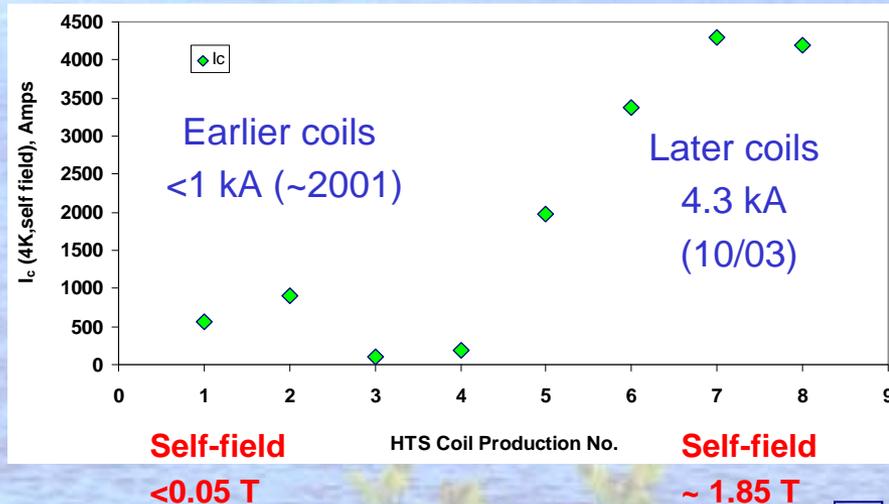


**HTS cables, coils & magnets can carry a significant current.**

**Cable made at LBL, reacted at Showa, tested at BNL**



**HTS coil wound & tested in a common coil magnet at BNL**



- **Experience with HTS R&D Magnets**
  - **RIA/FRIB Magnets (HTS for large heat loads)**
    - made with Bi2223 tape and now with YBCO Tape
  - **Common Coil Dipole (HTS for high field)**
    - made with Bi2212 Rutherford Cable
- **Future Possibilities for Accelerator Magnets**
  - **High Field Magnets**
    - with Bi2212 cable or YBCO *wide tape/* or *Roebel cable*
  - **Energy Efficient Magnets**
    - with YBCO Tape

## HTS now and in near future:

- Progress in US Bi2212 wire in last few years, and expected future support from DOE should make a significant difference
- Recent progress in YBCO is relevant to future prospects
  - Prices continue to fall and are likely to be well below what's expected from BSCCO
  - YBCO tape in many ways has superior performance to Bi2223
    - ✓ better mechanical properties
    - ✓ smaller bending radius possible with low degradation
    - ✓ expected higher engineering current density
    - ✓ Operating current of ~10 kA looks possible with wider tape (up to 40 mm rather than 4 mm) and/or with *Roebel cable*

# R&D on Roebel Cable in Europe (1)

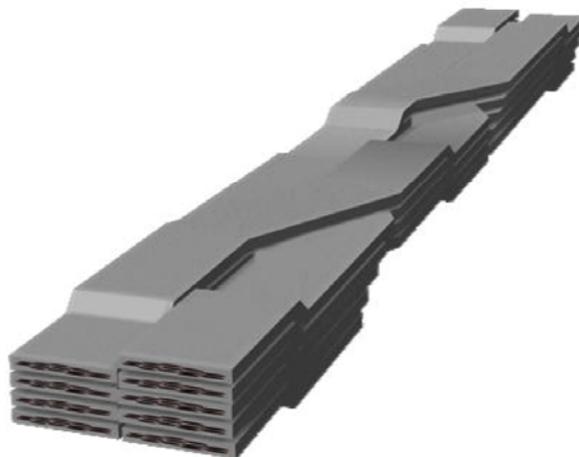
**Coupling and higher current (somewhat similar to that in Rutherford cable)**

**SIEMENS**

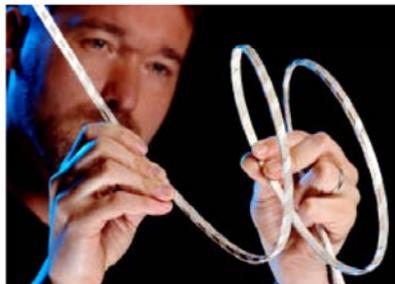
## Technical HTS-Conductors & HTS-Windings High Current Assemble

### Roebel bar conductor

- modular concept for high-current conductors
- transposed strands for low ac-loss
- insulated strands - thin coated plastics
- flexibility for coil winding
- long-lengths production - semiautomatic
- developed for HTS transformers
- presently not applicable for YBCO



Laboratory Cabling Facility LARA



Flexible conductor



13-strand conductor, length=160m

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WAMS2004\_SAG.ppt

**This was the case with BSCCO.**

**Expect similar in case of YBCO.**

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## Products

- HTS-Tapes
- Current Leads
- Coils
- **Roebel Conductors**

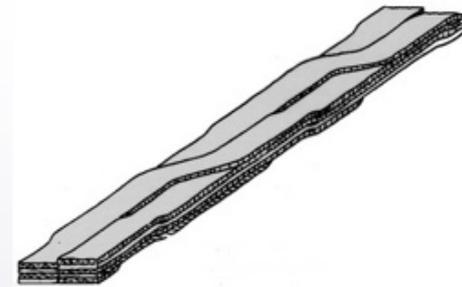
## Downloads

- BSCCO Data Sheet
- BSCCO AgAu Data Sheet
- YBCO Data Sheet
- EHTS Company Profile

## Search

### Roebel Conductors

are designed for high total currents. The transposition adds the advantage of equivalence of elementary tapes. This is of benefit for magnets as well as for AC applications (low loss). The Roebel conductors may be made by an odd number of transposed tapes, bare or insulated, the actual transposition scheme is usually designed to fit the requirements of the application. This cable has the advantage of high mechanical flexibility and high current at the same time.



## Helical winding with Roebel cable

## Roebel cable with YBCO

(SuperPower + Forschungszentrum)

- **Small bending radius (>11mm) possible**

Forschungszentrum Karlsruhe  
in der Helmholtz-Gemeinschaft

Forschungszentrum Karlsruhe  
in der Helmholtz-Gemeinschaft

Institut für Technische Physik, Superconducting materials, Wilfried Goldacker 8-20C

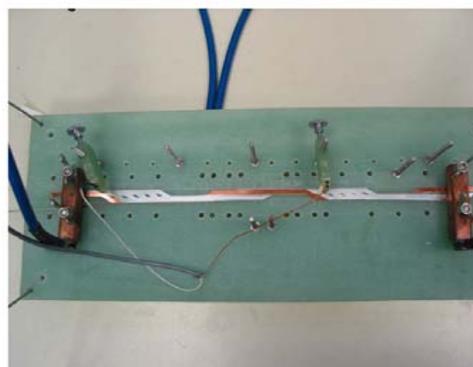
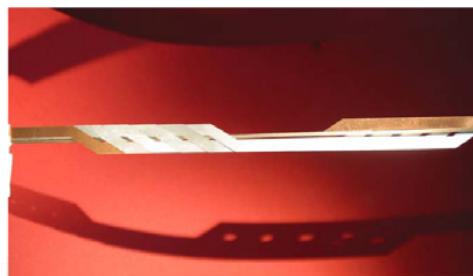
### 2. Step Full 16 strand DyBCO-RACC sample (35 cm length)



### 1. Step RACC – Cable with 5 CC – Strands + 1 Cu - strand

#### Results

- **Measured transport current  $I_c$  slightly above 300 Amps (approx. 305 Amps.)**
- Calculated  $I_c$  was 294 A
- $I_c$  onset was detected at 300 A (current source limit)
- Slight transport current increase through stabilising Cu strand ?
- Current sharing works !
- Ag cap layer (0.4 microns) seems to work sufficiently !
- External shunt of 1 mm<sup>2</sup> Cu ok !



pressed Indium sandwich contacts  
contact length 5 - 6 mm

No interstrand connection for first test

Parallel ext. Cu stabilizer with 5 mm<sup>2</sup>

Mixture of 2 CC batches: different Aa c

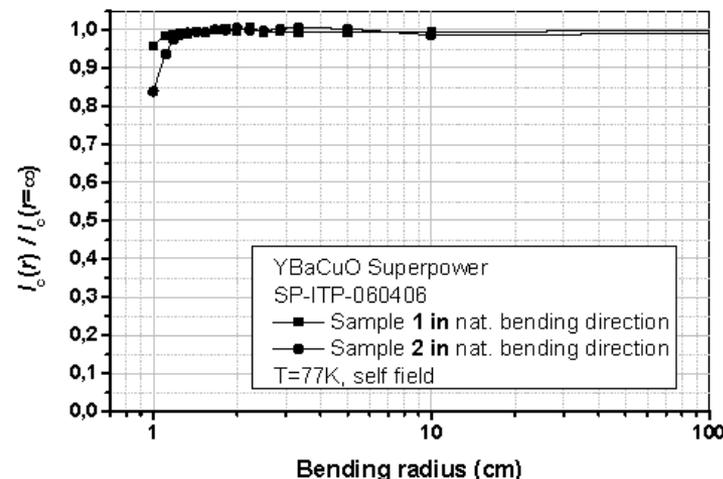


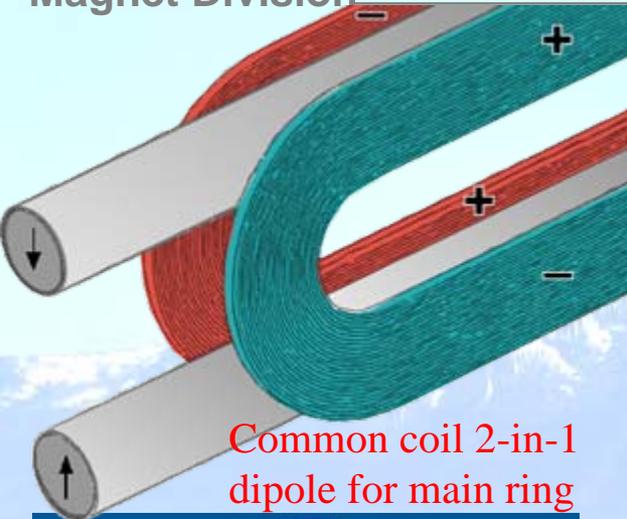
Fig. 3 Critical current of MOCVD SP CC with bending applied at 77 K

# ROEBEL Cable

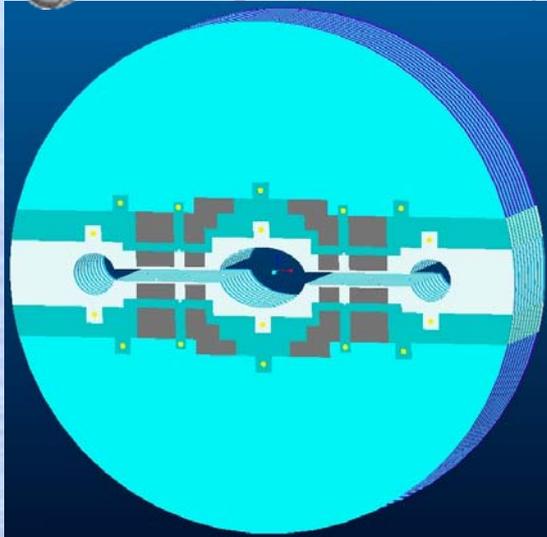
## An Interesting Topic for SBIR, etc.

- **Roebel cable may make YBCO tape much more attractive for accelerator and other type of magnets**
- **Roebel cable allows higher operating current and coupling between a number of wires (somewhat analogous to Rutherford cable with round wires)**
- **Roebel cable seems to be more attractive in racetrack coil designs. One can reference this cable R&D with various such designs (listed in next slide)**
- **Evaluate flexibility of Roebel cable with bending (in reference to cosine theta designs)**

# High Current, High Field, HTS Magnet Designs with Bi2212 Rutherford Cable and YBCO Roebel Cable



Common coil 2-in-1 dipole for main ring



Open midplane dipole for muon collider or LHC IR upgrade

- HTS is particularly attractive in very high field magnets – may be as an hybrid option in 20 T – 30 T designs.

- For React & Wind technology, racetrack coil magnet designs are more attractive.

- Possible designs :

- Common coil 2-in-1 dipole

- Single aperture dipole with lifted ends to clear bore tube

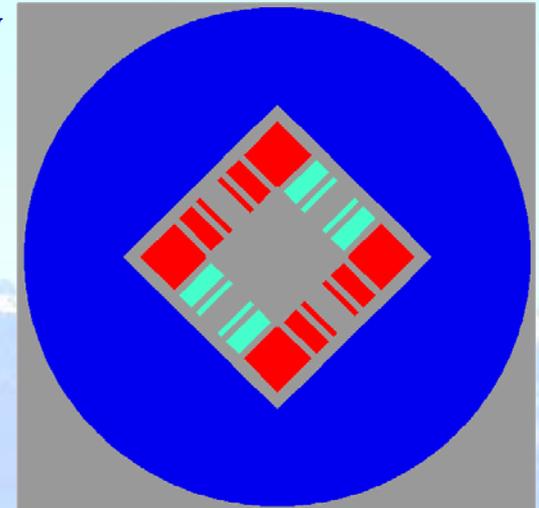
- Open midplane dipole

- Race-track coil quad

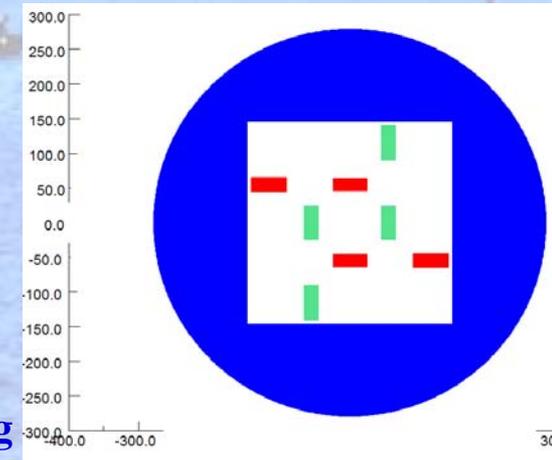
- Racetrack coil modular design

- For high luminosity IR, HTS is particularly attractive to face large energy deposition (RIA experience).

- For a few critical IR magnets, driving force should be performance and not the cost of the conductor.

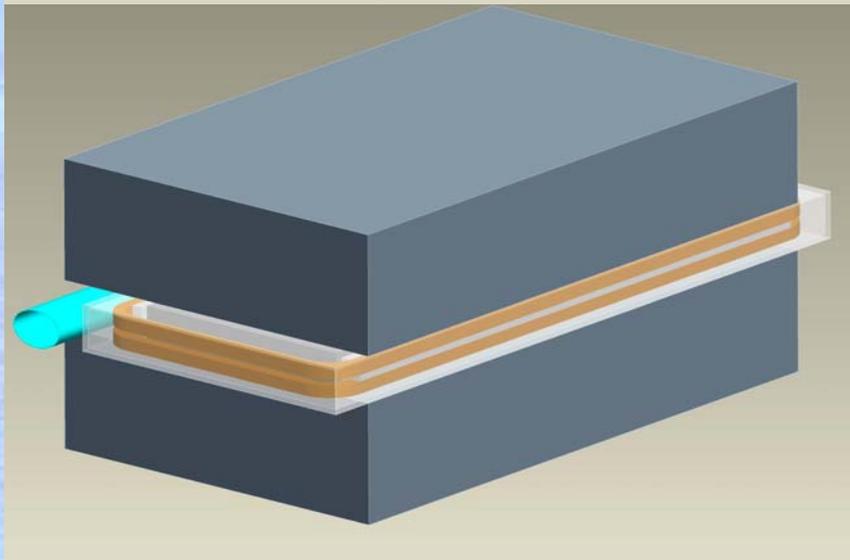
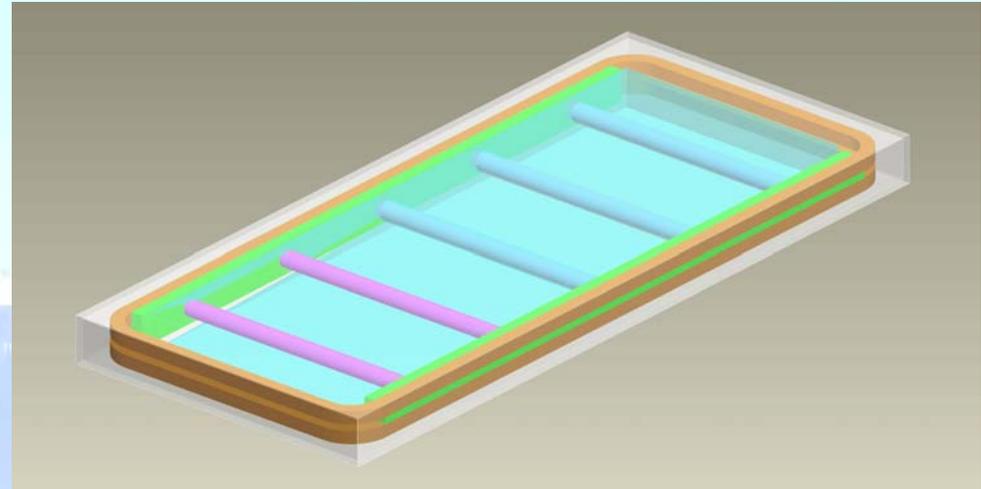
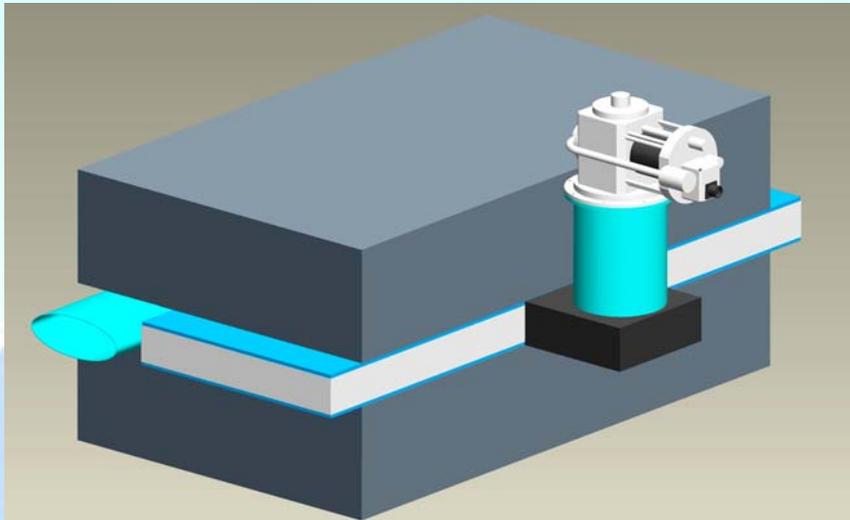


Racetrack coil quadrupole



Modular design for high gradient quadrupole

# Medium field (1.5 T-3 T) Energy Efficient HTS Magnets



- Consider the cost of ownership – capital cost for purchasing magnets and operating cost in light of increasing energy costs.
- With the cost of second generation conductor dropping, we have a good shot at this option if we can develop designs and technology that allows a lower cost magnet construction.

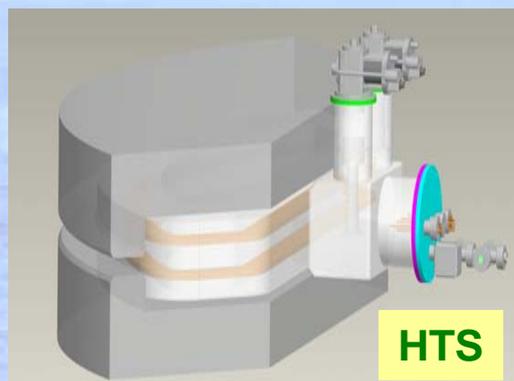
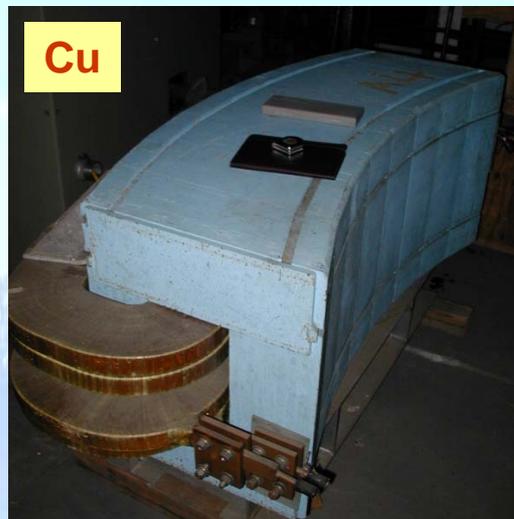
# A Case Study for Cost Comparison of Copper and HTS Dipole for Neutrino Facility

## Design Parameters:

- $B = 1.55 \text{ T}$
- $L = 3.73 \text{ m}$
- Pole width = 153 mm
- Pole gap = 76 mm

## Copper Magnets:

- Better known costs (estimated : ~150k\$ each for this magnet)
- Cost of individual components like coil, yoke, etc., is well understood
- High operating costs (estimated ~3 MW total)
- Low thermal conductivity water cooling plan
- Higher current (a few kA) power supply (higher cost)
- Maintenance issues (cost, downtime): water leak etc.



Desired cost of support structure and cryostat in this HTS magnet: < 20 K\$

## HTS Magnets:

- Develop designs to reduce cost (goal : ~150k\$/magnet for equivalent integral field)
- Cost of HTS as per present price: ~35 k\$ (only ~1/4, lower in future)
- Need to include cost of other components like iron (low and well understood), support structure, cryostat (major driver unless better designs developed)
- Lower operating costs (wall power of cryo-cooler?)
- Cost of cryo-coolers (compare with infrastructure cost of Low Thermal Conductivity Power Plant)
- Lower current (a few hundred Amp) power supply (cheaper)
- Maintenance issues (cost, downtime): cryo-coolers

# Summary and Outlook

- Successful construction and test of a number of coils and various configurations should encourage use of HTS in accelerator magnets.
- RIA R&D has demonstrated that HTS magnets can be designed, built and operated in presence of a large heat load environment.
- At present, HTS is particularly attractive for special applications (such as high field magnets, magnets that must deal with large energy deposition, etc.). These applications are driven by magnet performance and not the cost of the conductor.
- A larger scale application of HTS may lie in the magnets for beam-lines, low energy machines (such as injectors, neutrino factories and synchrotron radiation sources to save operating costs – electricity) and magnets for a number of medical applications.
- Second generation conductor should make HTS magnets much more attractive (higher  $J_e$ , lower cost and higher temperature operation).