

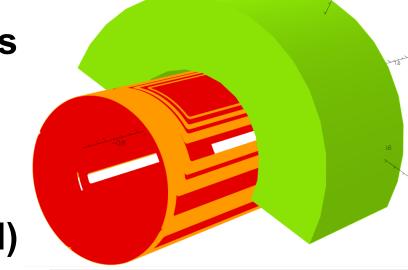
### **Major Goals of the 1st Update**

- Add dipole on the preferred 6-layer (three coil sets) design to make the field on the electron beam path (x=-34 mm) zero and make oscillation (up-down variation in the vertical field) <1 kG (present serpentine design has ~100 G).
- Compute new margin for the integral field on the integral path of the center of proton beam is ~1.56 T.m at x=126 mm and 25 mRad angle.
- Perform the margin calculations for the most ambitious case of the optimum integral design with 6 superconductors around 1 copper and do it for both 1.92 K and 4.2 K.

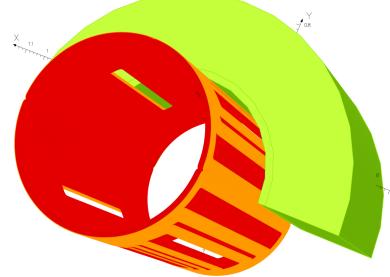


Dipole Coil Added to the Quad in B0PF

- Dipole coil runs in series with the quad and is made with the same cable as the quad coil.
- A single layer is enough (optimum integral design can have a single layer, as in the optimum integral corrector in the AGS tunnel)
- Even a single layer design creates too much field, and therefore more than ½ of the turns are removed to avoid over-correction.
- Turns are clubbed together in a few blocks (rather than evenly distributing the gaps between them) to save the construction time.

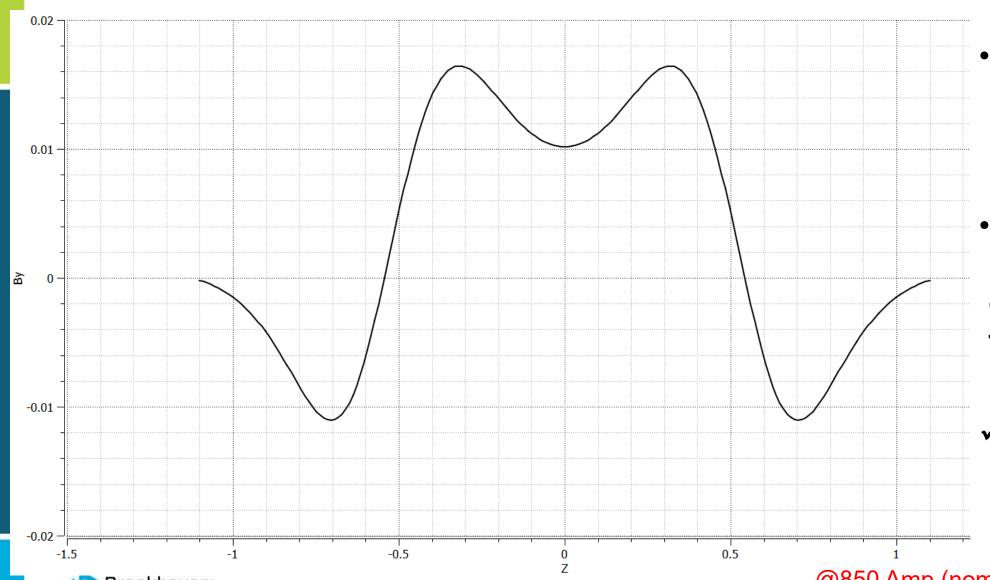








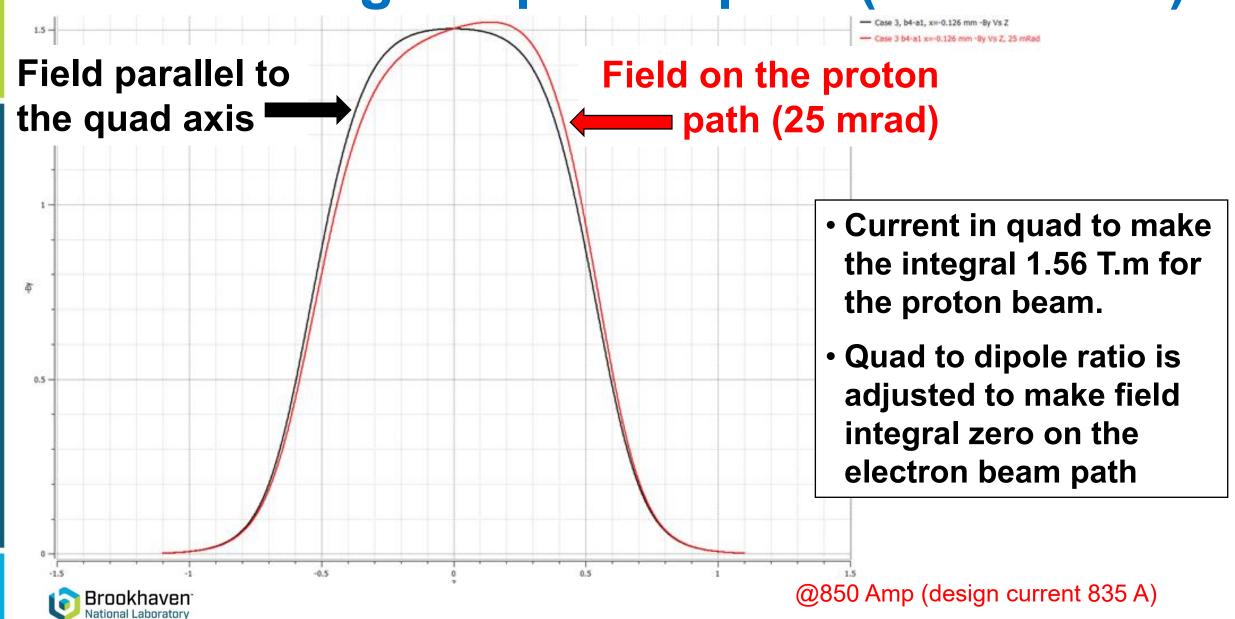
### Field along the electron path (X=-34 mm)



- Integral field is nearly zero (can be fine tuned to make it exactly 0)
- •Oscillation in By is naturally <1 kG or 0.1 T (may be further reduced if necessary).
- ✓ Good enough for the initial investigation

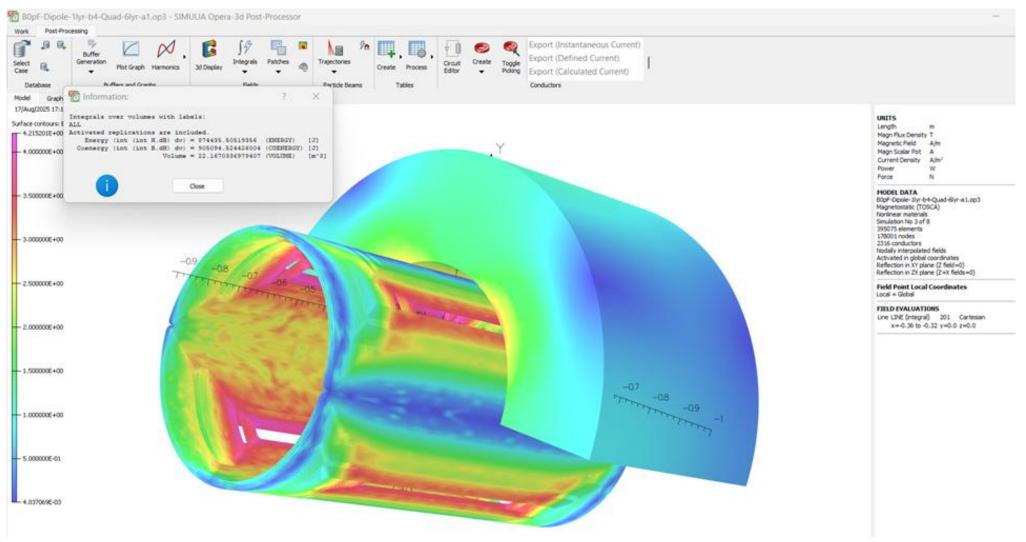
@850 Amp (nominal 835A)

### Field along the proton path (X=126 mm)



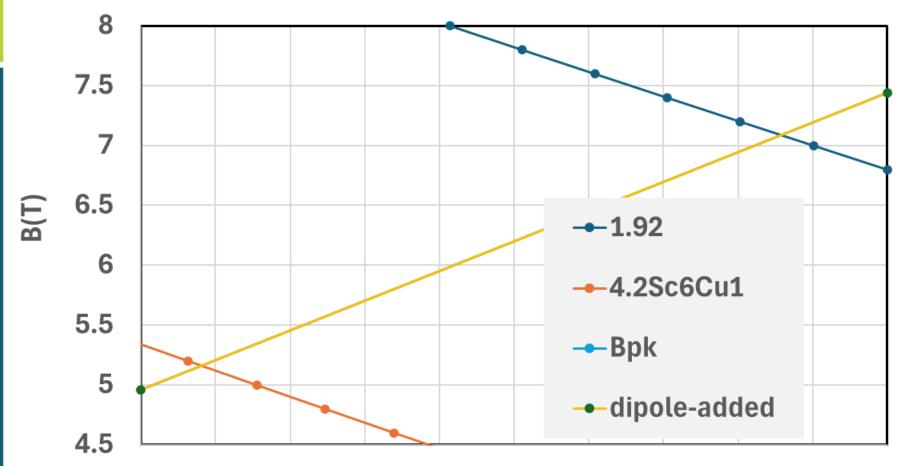
**Magnet Division** 

# Model with field Superimposed at 850 A (nominal current for desired integral is 835 A)





### 6-Layer Optimum Integral Design B0pF Quad Performance (with 1-layer optimum integral dipole for electron beam)



**Nominal Current** for design integral: 830 A

SS@1.92K, all SC 1460 Amp (margin = 75%)

SS@4.2K, 6SC on 1Cu: 1040 Amp (margin = 25%)

1000 1050 1100 1150 1200 1250 1300 1350 1400 1450 1500 I(A)



# Summary

- A sparsely packed single-layer optimum integral dipole was sufficient to obtain zero integral field on the path of electron beam in 6-layer B0PF Quad.
- The first design itself produced a peak-to-peak variation of ¼ kG or 0.025 T (goal was to make it 1 kG or 0.1 T).
- All essential advantages that were presented in the 1<sup>st</sup> quick design last week, are still retained in the same optimum integral 6-layer quad. These include: (a) possibility of testing it to the design performance at 4.2 K with a respectable 25% margin, (b) allowing central wire to become copper for better quench protection, in addition to reducing current to ~835 Amp from the 1146 A.
- Next step: try to make it a combined function design 6-layer design which creates both dipole and quadrupole.
- Further steps: A quick quench analysis and winding of short ¼ coil.



### Extra slides

(selected slides from the presentation on 8/14)



### Background

The inset slide must force one to at least have a quick look at the optimum integral design for B0pF (reference for length to id ratio: <4 in quad; it's 1.8 here). However, to change from the serpentine design to anything else at this stage, the benefits must be significant, such as (at least one or two from the list below):

#### **Loss in Integral Field Due to Ends and Some Short EIC Magnets**

- Relative loss starts becoming important when the length of magnet is so small that the straight becomes comparable to the ends.
- Typical mechanical length of end: ~ 2 coil diameter each in dipole. Total ends in dipole: ~four diameter (~2 coil diameter in quad).
- Compare coil length (L) to coil i.d. (id) ratios. Relative loss will be significant when the ratio is <8 in dipoles and <4 in quadrupoles.

#### Coil length to coil diameter ratios in some EIC magnets:

- > B0ApF (L = 600 mm, id = 114 mm): ~5.3
- $\triangleright$  B1ApF (L = 1600 mm, id = 370 mm): ~4.3
- ▶ B1pF/B1ApF (L = 2500 mm, id = 363 mm): ~6.9
- ➤ B0pF/Q0eF (L=1200 mm, id = 656 mm): ~1.8 (refer to quad)

Update on the Optimum Integral Design for B0pF

Optimum Integral Design for EIC -Ramesh Gupta Magnet Steering Group Meeting July 25, 2025

- 6 layers instead of 8 layers so that it can be tested in our Dewar at 4K (beside cutting cost and schedule).
- The magnet achieves the design field integral at 4.2 K (with a good margin) to demonstrate the design.
- **Quench protection becomes** significantly less challenging.
- > Max. field gradient (Lorentz forces) gets reduced significantly.

Following slides are from <2 days of work using the same cable as in serpentine. First look is promising!

Reference quide

~8 in dipole

~4 in guads



# Six superconductor around one copper in 6-around-1 cable (instead of all super)

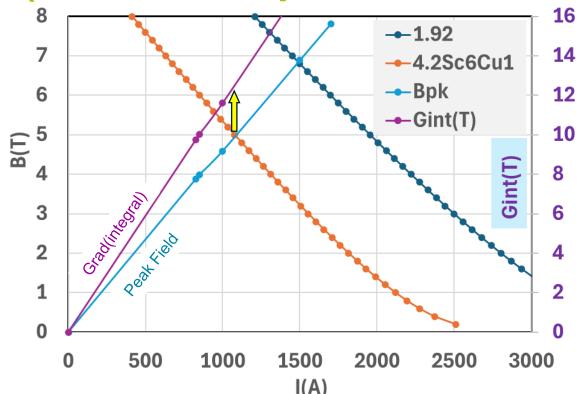
- Center wire in 6-around-1 cable is not transposed.
- This creates issues at high ramp rates as the center wire tries to resist the change. At very high ramp rates, the current can even be in a direction opposite to the transport current. That will reduce the quench current of the magnet.
- It, however, should also help in quench protection due to the "quench back" effect. The center wire can be copper.
- Making the center wire Cu effectively increases the copper to superconductor ratio. That will not only help in quench protection but may even prevent a quench.
- The penalty to pay is in reduction in the critical current of the cable which becomes 6/7 of that in all super wire case.

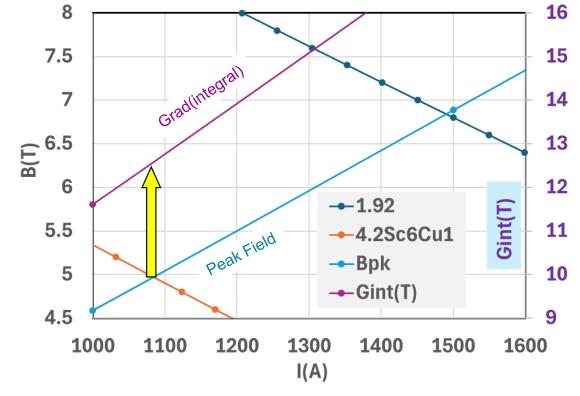


Cu/Sc from Brucker			
Original	Cu/Sc	1.75	
Cu wires	1		
SC Wires	6		
Wire dia	0.473	mm	
Wire area	0.176	mm^2	
Super in wire	0.064	mm^2	
Cu in Wire	0.112	mm^2	
Cable Area	1.230	mm^2	
Cu in Cable	0.847	mm^2	
Super in cable	0.383	mm^2	
<b>Effective</b>	Cu/Sc	2.21	
Iquench	1080	Amp	
Jcu@Qnch	1276	A/mm^2	
Idesign	827	Amp	
Jcu@design	977	A/mm^2	

### 6-layer Optimum Integral Design for B0PF

(all seven super at 1.92 K Vs six super and one cu at 4.2 K)





#### **Ultimate comparison**

(for reference present serpentine design has 8 layers, 1143 A and 43% margin at 1.92 K for all seven super)

Still heathy margins despite granting all wishes!

#### Design current 827 A

	Iss(A)	Margin(%)
All SC @1.92K	1490	<b>80</b> %
SC6Cu1@4.2K	1090	<b>32</b> %

-Ramesh Gupta

August 18, 2025

## Summary and the Next Step (1)

- Let us compare the two options. The current serpentine design has eight quad and two dipole layers. Even quad doesn't fit in the Dewar.
- It has a nominal operating current of 1143 A. It has a margin of 43% at 1.92 K when all wires in 6-around-1 are superconducting wire, same as always.
- A quench protection solution has been found for the serpentine design with ten sets of leads and dump registers. It, however, is in challenging territory.
- Initial optimum integral design has 6 layers in quad. It can fit in our Dewar for 4.2 K testing for a computed short sample that has a comfortable 32% margin.
- Moreover, the center wire is made of copper to help quench protection by taking advantage of the quench back. This also increases Cu/Sc ratio to 2.2 to reduce current density in copper after quench at the design current, which was already smaller in this optimum integral design (827 A instead of 1143 A).



## Summary and the Next Step (2)

- Lower maximum gradient means lower Lorentz forces, which should make the design less challenging. We may be able to reduce the thickness of inner tube.
- Initial outcome looks very promising. However, the electro-magnetic design, etc., must be analyzed independently (e.g. Vikas with RAT). In parallel a more optimized version can be found. This should be a few days activity only.
- Then a quick 1<sup>st</sup> order quench analysis of this design should be performed.
- Optimum integral design can conveniently allow a combined function design (rather than quad and dipole in series) – hopefully still in a 6-layer design.
- As attractive as that option maybe, evaluation of that may wait a bit for now.
  However, if that works, we will need only 6 sets of leads and dump resistors
  (instead of 10) and should offer a better technical and strategic option, in
  addition to all above.

